TECHNICAL GUIDE - CANADA

## TECH GUIDE

| PWI 18 S
| PWI 205
| PWI 32S
| PWI 36L
| PWI 42S
| PWI 52S
| PWI 56L
PWT I-JOIST

RESIDENTIAL CONSTRUCTION

PWT FOCUSED ON EWP

## PWT <br> FOCUSED ON EWP

PWT ${ }^{\text {TM }}$ I-Joists are straighter and more uniform in strength, stiffness and size than traditional lumber, providing a strong, sturdy floor. We offer longer lengths so that ceilings and floors can be designed with fewer pieces, saving time on installation. Other advantages over lumber include lower moisture content, which makes our I-Joists less likely to split, shrink, twist, warp or bow. This means reduced callbacks due to fewer pops and squeaks.

## Strength in Numbers

The full range of PWT products are designed and manufactured to install easily and work together to provide a strong, sound structure.

For I-Joists, we combine laminated veneer lumber (LVL) or finger-jointed sawn lumber flanges with a web of oriented strand board (OSB) to produce an I-shaped structural member. The webs allow plumbing and wiring to pass through without extra framing, while the flanges resist bending - ideal for long spans in floors, ceilings and roofs.
PWT I-Joists are a building material with built-in environmental benefits

- Made of engineered wood substrate, a renewable resource with a reduced environmental impact
- Raw material procurement targets small, fast growing trees
- Only low-emitting, safe resins are used as a binder
- Available in longer lengths, reducing the number of pieces needed; this results in more efficient utilization of resources
- Can help you qualify for certification points in a number of leading green building programs


## Peace-of-Mind for a Lifetime

If your PWT I-Joists ever develop performance problems due a manufacturing deflect, PWT will cover all reasonable repair and/or replacement costs per the conditions of our Lifetime Limited Warranty. Visit pwtewp.com to view our complete warranty, or contact your local PWT distributor or sales office for an original copy.

## Compliant with Major Building Codes

PWT I-Joists have been evaluated by CCMC for compliance with the National Building Code of Canada. Contact your local PWT distributor or visit pwtewp.com for the most current code reports.

## Lifetime Limited Warranty

Products are backed by a lifetime limited warranty. Visit pwtewp.com or call (800) 515-7570 for a copy of the warranty.


## I-JOIST

## |-Joists

PWI 18S / LPI 18 Width: $2-1 / 2^{1 "}$ Depths: 9-1/2", 11-7/8" Web Thickness: 3/8" Flange Materia: Solid Sawn Flange Depth: 1-1/2"

PWI 20S / LPI 20Plus
Width: 2-1/2"
Depths: 9-1/2", 11-7/8", 14", $16^{" 1}$
Web Thickness: 3/8"
Flange Material: Solid Sawn
Flange Depth: 1-1/2"
PWI 32S / LPI 32Plus
Width: 2-1/2"
Depths: $9-1 / 2^{\prime \prime}, 11-7 / 8^{\prime \prime}, 14^{\prime \prime}, 16^{\prime \prime}$
Web Thickness: $3 / 8^{\prime \prime}$
Flange Material: Solid Sawn
Flange Depth: 1-1/2"
PWI 36L / LPI 36
Width: 2-1/4"
Depths: 11-7/8", 14", $16^{\text {" }}$
Web Thickness: 3/8"
Flange Material: LVL
Flange Depth: 1-1/2"

Code Evaluation Reports:
CCMC evaluation reports can be obtained at www._nre-chrc.sc.ca.

CCMC 12412-R, APA PR-L238C or visit pwtewp.com

## Product Specifications \& Design Values

LIMIT STATES DESIGN VALUES

| Series | Depth | Weight (plf) | Factored Moment (lb-ft) | $\underset{\left(\mathrm{bl}-\mathrm{in}^{2}\right)}{\mathrm{El}\left(0^{6}\right)}$ | $K\left(x 10^{6}\right)$ (lb-ft/in) | Factored Shear (Ibs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PWI 18S, LPI 18 | 9-1/2" | 2.6 | 3760 | 142 | 0.355 | 1785 |
|  | 11-7/8" | 2.9 | 4450 | 248 | 0.435 | 2105 |
| PWI 20S, LPI 20Plus | 9-1/2" | 2.6 | 4670 | 185 | 0.358 | 1990 |
|  | 11-7/8" | 2.9 | 6250 | 318 | 0.438 | 2345 |
|  | $14 "$ | 3.1 | 7320 | 474 | 0.512 | 2650 |
|  | $16^{\prime \prime}$ | 3.3 | 8400 | 652 | 0.582 | 2950 |
| PWI 32S, LPI 32Plus | 9-1/2" | 2.6 | 5570 | 221 | 0.358 | 1990 |
|  | 11-7/8" | 2.9 | 7210 | 375 | 0.438 | 2345 |
|  | 14 " | 3.1 | 8680 | 549 | 0.512 | 2650 |
|  | $16 "$ | 3.3 | 10065 | 743 | 0.582 | 2950 |
| PWI 36L, LPI 36 | 11-7/8" | 3.1 | 10715 | 429 | 0.468 | 2550 |
|  | 14" | 3.4 | 12900 | 622 | 0.550 | 2890 |
|  | $16 "$ | 3.6 | 14960 | 836 | 0.625 | 3190 |
| PWI 42S, LPI 42Plus | 9-1/2" | 3.4 | 8940 | 321 | 0.412 | 2115 |
|  | 11-7/8" | 3.5 | 11585 | 547 | 0.515 | 2565 |
|  | 14 " | 3.8 | 13950 | 802 | 0.607 | 2960 |
|  | $16 "$ | 4.0 | 16180 | 1092 | 0.693 | 3340 |
| PWI 52S, LPI 52Plus | 11-7/8" | 4.5 | 14085 | 600 | 0.633 | 3245 |
|  | $14{ }^{\prime \prime}$ | 4.8 | 16960 | 874 | 0.747 | 3680 |
|  | 16" | 5.0 | 19670 | 1183 | 0.853 | 4080 |
| PWI 56L, LPI 56 | 11-7/8" | 4.5 | 16920 | 668 | 0.549 | 3245 |
|  | $14{ }^{\prime \prime}$ | 4.8 | 20370 | 968 | 0.641 | 3680 |
|  | 16" | 5.0 | 23625 | 1301 | 0.729 | 4080 |

FACTORED REACTION AND BEARING RESISTANCE

| Series | Depth | End Reaction Resistance ${ }^{1}$ (lbs) |  |  |  | Interior Reaction Resistance ${ }^{1}(\mathrm{lbs})$ |  |  |  | Flange Bearing Resistance, Ø $\mathrm{F}_{\mathrm{cp}}(\mathrm{lb} / \mathrm{in})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Minimum Bearing ( $11 / 2$ ) |  | Maximum Bearing (4") |  | Minimum Bearing ( $31 / 2 \mathrm{~L}$ ) |  | Maximum Bearing ( $51 / 2 \mathrm{~L}$ ) |  |  |
|  |  | Without Stiffeners | With Stiffeners | Without Stiffeners | $\begin{gathered} \text { With } \\ \text { Stiffeners } \end{gathered}$ | Without Stiffeners | With Stiffeners | Without Stiffeners | $\begin{gathered} \text { With } \\ \text { Stiffeners } \end{gathered}$ |  |
| PWI 18S, LPI 18 | 9-1/2" | 1375 | 1620 | 1570 | 1785 | 3115 | 3370 | 3480 | 3740 | 1380 |
|  | 11-7/8" | 1375 | 1805 | 1640 | 2105 | 3305 | 3585 | 3685 | 4015 |  |
| PWI 20S, LPI 20Plus | 9-1/2" | 1530 | 1800 | 1750 | 1990 | 3465 | 3750 | 3865 | 4160 | 1380 |
|  | 11-7/8" | 1530 | 2010 | 1830 | 2345 | 3680 | 3985 | 4095 | 4465 |  |
|  | $14 "$ | 1530 | 2200 | 1895 | 2650 | 3875 | 4205 | 4300 | 4745 |  |
|  | $16 "$ | 1530 | 2385 | 1955 | 2950 | 4055 | 4410 | 4500 | 5010 |  |
| PWI 32S, LPI 32Plus | 9-1/2" | 1530 | 1800 | 1750 | 1990 | 3465 | 3750 | 3865 | 4160 | 1695 |
|  | 11-7/8" | 1530 | 2010 | 1830 | 2345 | 3680 | 3985 | 4095 | 4465 |  |
|  | 14 " | 1530 | 2200 | 1895 | 2650 | 3875 | 4205 | 4300 | 4745 |  |
|  | $16 "$ | 1530 | 2385 | 1955 | 2950 | 4055 | 4410 | 4500 | 5010 |  |
| PWI 36L, LPI 36 | 11-7/8" | 1620 | 2370 | 2030 | 2550 | 3940 | 4900 | 4475 | 5475 | 1720 |
|  | 14 " | 1620 | 2390 | 2090 | 2890 | 3940 | 5060 | 4475 | 5625 |  |
|  | $16 "$ | 1620 | 2405 | 2145 | 3190 | 3940 | 5215 | 4475 | 5770 |  |
| PWI 42S, LPI 42Plus | 9-1/2" | 1870 | 2115 | 2060 | 2115 | 4575 | 4885 | 4640 | 5045 | 2450 |
|  | 11-7/8" | 1965 | 2385 | 2520 | 2565 | 4775 | 5270 | 4925 | 5550 |  |
|  | 14 " | 2050 | 2620 | 2520 | 2960 | 4955 | 5625 | 5175 | 6005 |  |
|  | $16^{\prime \prime}$ | 2130 | 2840 | 2520 | 3340 | 5120 | 5960 | 5420 | 6440 |  |
| PWI 52S, LPI 52Plus | 11-7/8" | 2160 | 2875 | 2670 | 3245 | 5400 | 6315 | 5740 | 6645 | 2450 |
|  | $14{ }^{\prime \prime}$ | 2185 | 3110 | 2910 | 3680 | 5420 | 6725 | 5910 | 7165 |  |
|  | $16 "$ | 2210 | 3330 | 3135 | 4080 | 5445 | 7110 | 6075 | 7665 |  |
| PWI 56L, LPI 56 | 11-7/8" | 1805 | 2620 | 2390 | 3245 | 4940 | 6090 | 5795 | 6410 | 2720 |
|  | $14{ }^{\prime \prime}$ | 1805 | 2770 | 2425 | 3680 | 4940 | 6400 | 5795 | 6785 |  |
|  | $16 "$ | 1805 | 2910 | 2455 | 4080 | 4940 | 6700 | 5795 | 7140 |  |

## Notes:

1. End and Interior Reaction Capacity shall be limited by the Flange Bearing Capacity or the bearing capacity of the support material, whichever is less.
2. The Flange Bearing Capacity, per inch of bearing length, is based on the allowable compression perpendicular-to-grain of the l-Joist flange, accounting for eased edges.
3. To account for edge easing when determining the bearing capacity of the support material, subtract 0.25 " from the flange width for the PWI 18S, PWI 20S, PWI 32S, PWI 42S \& PWI 52S; LPI 18, LPI 20Plus, LPI 32Plus, LPI 42Plus \& LPI 52Plus, and subtract 0.10" from the flange width for the PWI 36L \& PWI 56L; LPI 36 \& LPI 56.
4. Reaction Resistance, Flange Bearing Resistance and the bearing resistance of any wood support are for standard load duration and shall be reduced according to code for longer loading duration.
5. Reaction Resistance and Flange Bearing Resistance may be increased over that tabulated for the minimum bearing length. Linear interpolation of the Reaction Resistance between the minimum and maximum bearing length is permitted. Bearing lengths longer than the maximum do not further increase Reaction Resistance. Flange Bearing Resistance and that of a wood support will increase with additional bearing length.
6. The Interior Reaction Resistance may be calculated to a minimum bearing length of 3 inches, based on the $3-1 / 2^{\prime \prime}$ and $5-1 / 2^{\prime \prime}$ values.
7. See page 25 for information on web stiffener sizes and nailing.

Notes:

1. PWT I-Joists shall be designed for dry-use conditions only. Dry-use applies to products installed in dry, covered and well ventilated interior conditions in which the average equilibrium moisture content (MC) of lumber is $15 \%$ or less over a year and does not exceed 19\% at any time.
2. Moment and Shear are the factored resistances for standard load duration and shall be adjusted according to code.
3. Moment resistance shall not be increased for repetitive member use.
4. Deflection calculations shall include both bending and shear deformations.
Deflection for a simple span, uniform load:

$$
\Delta=\frac{22.5 W L^{4}}{E l}+\frac{W L^{2}}{K}
$$

Where: $\Delta=$ deflection (in)
w = uniform load (pif)
L = design span (ft)
$\mathrm{El}=$ bending stiffness (from table)
$\mathrm{K}=$ shear stiffness (from table)

Equations for other conditions can be found in engineering references.


Example: Determine the stiffened end reaction capacity for a 14 " PWI 325 with 2" of bearing for a non-snow roof load and supported on an SPF wall plate (768 psi).

1. Determine End Reaction (ER) w/Stiffeners: $E R=2200+(2650-2200)$ $\left(2^{\prime \prime}-1.5^{\prime \prime}\right) /\left(4^{\prime \prime}-1.5^{\prime \prime}\right)=2290 \mathrm{lbs}$
2. Determine Flange Bearing Resistance (FBR): $F$ FBR $=1695 \mathrm{lb} / \mathrm{in}^{*} 2^{\prime \prime}=3390 \mathrm{lbs}$
3. Determine wall Plate Bearing Resistance (PBR): PBR $=0.8^{*} 768$ psi * (2.5" $\left.-0.25^{\prime \prime}\right)^{\star}$ $2^{\prime \prime}=2764$ lbs
4. Final End Reaction Resistance w/Stiffeners $=2290 \mathrm{lbs}$

# Floor Span Tables: 19/32 OSB Sheathing Specified Floor Loads: 40 PSF Live Load, 15 PSF Dead Load 

## Table Usage:

1. Select the appropriate table based on the floor system construction.
2. Select the Simple Span or Continuous Span section of the table, as required.
3. Find a span that meets or exceeds the required clear span.
4. Read the corresponding joist series, depth and spacing.

Caution: For floor systems that require both simple span and continuous span joists, it is a good idea to check both before selecting a joist. Some conditions are controlled by continuous span rather than simple span.


## 19/32 OSB SHEATHING NAILED ONLY

| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  | Direct Attached 1/2" Gypsum Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  | Maximum Continuous Spans |  |  | Maximum Simple Spans |  |  | Maximum Continuous Spans |  |  |
|  |  | 12" 00 | 16" OC | 19.2" oc | 12" Oc | 16" OC | 19.2" oc | 12" OC | 16" oc | 19.2" oc | 12" oc | 16" Oc | 19.2" oc |
| PWI 18S, LPI 18 | 9-1/2" | 13'6" | 12'-7" | $12^{\prime}-1{ }^{\prime \prime}$ | 14'0" | 13'0" | 12'-6" | 14'0" | 13'0'0' | $12^{\prime \prime} 6^{\prime \prime}$ | 14'5'5' | 13'-5" | 12'-11" |
|  | 11-7/8" | $15^{\prime}-4$ " | $14^{\prime}-4{ }^{\prime \prime}$ | 13'-9" | 15'-10" | 14'-9" | $14^{\prime}-2^{\prime \prime}$ | 15'-10" | 14'9" | $14^{\prime}-2{ }^{\prime \prime}$ | $16^{\prime}-5 "$ | 15'-3" | 14'-8" |
| PWI 20S, LPI 20Plus | 9-1/2" | 14'4" | $13^{\prime \prime} \mathbf{4}^{\prime \prime}$ | 12'-10" | 14'-9" | 13'9" | 13'-3' | 14'9" | 13'9" | 13'-2' | 15'3' | 14'-2' | 13'7" |
|  | 11-7/8" | $16^{\prime \prime} 2^{\prime \prime}$ | 15 '1" | 14'-5" | 16'9" | 15'7" | 14'-11" | 16'7" | 15'6" | 14'-10" | $17^{\prime}-3{ }^{\prime \prime}$ | 16'-1' | 15'-5" |
|  | 14 " | $17^{\prime \prime}$-8' | $16^{\prime}-5{ }^{\prime \prime}$ | 15'-10" | 18'-5" | 17'-0" | $16^{\prime}-4 "$ | 18'3" | $16^{\prime}-11^{\prime \prime}$ | $16^{\prime}-3 "$ | 19'2' ${ }^{\prime \prime}$ | 17'7" | $16^{\prime}-10^{\prime \prime}$ |
|  | $16^{\prime \prime}$ | 19'-3" | $17^{\prime}-8{ }^{\prime \prime}$ | 16'-11" | 20'3" | 18'6" | $17^{\prime}-7{ }^{\prime \prime}$ | 20'0" | 18'-4" | $17^{\prime}-6{ }^{\prime \prime}$ | 21-0" | 19'-3" | 18'-3" |
| PWI 32S, LPI 32Plus | 9-1/2" | 14'-10" | 13'10" | 13'-3" | 15'4" | 14'4" | 13'-9" | 15'3" | 14'-2" | 13'-7" | 15'9" | 14'-8" | $14^{\prime}-1{ }^{\prime \prime}$ |
|  | 11-7/8" | 16'-9" | $15 ' 7{ }^{\prime \prime}$ | 14'-11" | 17-4" | $16^{\prime}-1{ }^{\prime \prime}$ | 15'-6" | 17-2" | 16'0" | 15'-4" | $17^{\prime}-10^{\prime \prime}$ | 16'7" | 15'-11" |
|  | 14 " | 18'3" | 16'-11" | $16^{\prime}-3 "$ | 19'-2" | 17'7" | 16'10" | 18'-11" | 17'-5" | 16'-9" | 19'-11" | 18'-2" | 17-4" |
|  | $16^{\prime \prime}$ | 19'-11" | $18^{\prime}-2{ }^{\prime \prime}$ | $17^{\prime \prime}-5^{\prime \prime}$ | 20'-11" | 19'1" | 18'-2" | 20'8" | 18'-11" | 17'-11" | 21-9" | 19'-10" | $18^{\prime}-10^{\prime \prime}$ |
| PWI 36L, LPI 36 | 11-7/8" | 17'-3" | 16'-1" | 15'-5" | 17'-10" | 16'7" | 15'-11" | 17'-8" | 16'6" | 15'-9" | 18'-6" | 17'-1" | $16^{\prime}-4$ " |
|  | $14^{\prime \prime}$ | 18-11" | $17^{\prime}-5{ }^{\prime \prime}$ | 16'-9" | 19'-11" | 18'2" | 17-4" | 19'-7" | 17'-11" | $17^{\prime}-2{ }^{\prime \prime}$ | 20'7" | 18'-10" | 17'-10" |
|  | $16 "$ | 20'8" | 18'-10" | 17'-11" | 21'-8" | 19'9" | 18-9" | 21'-4" | 19'-6" | $18^{\prime}-6 "$ | 22'5" | 20'6" | 19'-6" |
| PWI 42S, LPI 42Plus | 9-1/2" | $16^{\prime}-1{ }^{\prime \prime}$ | 15'0" | 14'-5" | $16^{\prime}-8^{\prime \prime}$ | 15'7" | 14'-11" | 16'-6" | 15'4" | 14'-9" | 17'-1' | 15'-11" | 15'3" |
|  | 11-7/8" | 18'3" | 16'-11" | 16'-3" | 19'-2" | 17'-7" | 16'10" | 18'9" | 17'-4" | $16^{\prime}-7{ }^{\prime \prime}$ | 19'-9" | 18'-0" | 17'-3" |
|  | $14$ | 20'-4" | 18'7" | $17^{\prime}-8{ }^{\prime \prime}$ | 21'-5" | 19'6" | 18'6" | 21'0" | 19'-2" | 18'-2" | 22'-1' | 20'-2" | 19'-1" |
|  | $16 "$ | 22'-3" | $20^{\prime \prime} 4^{\prime \prime}$ | $19 \cdot{ }^{\prime \prime}$ | 23'5" | 21'-4" | 20'3" | 22'-11" | 21'0" | 19'-11" | 24'-1' | 22-1" | 20'-11" |
| PWI 52S, LPI 52Plus | 11-7/8" | 18-10" | 17'-5" | 16'8" | 19'9" | 18'1" | 17'-4" | 19'-5" | 17'-9" | 17'-1" | 20'-4" | 18'7" | 17'-8" |
|  | $14 "$ | 21'0" | 19'-3" | 18'-3" | 22'-1" | 20'2" | 19'-2" | 21'-7" | 19'-9" | 18'9" | 22'-9" | 20'9" | 19'-9" |
|  | $16 "$ | 22'-11" | 20'-11" | 19'-11" | 24'-1" | 22'0" | 20'-11" | 23'7" | 21'-7" | 20'6" | $24^{\prime}-10^{\prime \prime}$ | 22'-8" | 21'-6" |
| PWI 56L, LPI 56 | 11-7/8" | 19'-3" | 17'-8" | 17'-0" | 20'3" | 18'6" | 17'-7" | 19'-10" | 18'1" | 17-4" | 20'10" | 19'0" | 18'-1" |
|  | $14^{\prime \prime}$ | 21'5" | 19'-7" | 18'7" | 22'-7" | 20'7" | 19'-6" | 22'-1" | 20'2" | 19'1" | 23'-2" | 21-2" | 20'-1" |
|  | $16 "$ | 23'-4" | 21'-4" | $20^{\prime}-3 "$ | 24'-7" | 22'-5" | 21'-3" | 24'0" | 22'0" | 20'10" | 25'-3' | 23'-1' | 21'-11" |

## 19/32 OSB SHEATHING GLUED \& NAILED

| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  | Maximum Continuous Spans |  |  |
|  |  | 12" oc | 16" OC | 19.2" OC | 12" OC | 16" oc | 19.2" oc |
| PWI 18S, LPI 18 | 9-1/2" | 14'-10" | 14'0" | 13'7" | 15'4" | 14'-6" | 14'-0" |
|  | 11-7/8" | $16^{\prime}-8{ }^{\prime \prime}$ | 15'9" | 15'3" | 17'-3" | 16'3" | 15'9" |
| PWI 20S, LPI 20Plus | 9-1/2" | 15'-5" | 14'-7" | 14'1" | 15'-11" | 15'0" | 14'-7" |
|  | 11-7/8" | $17^{\prime}-4{ }^{\prime \prime}$ | $16^{\prime}-4 "$ | 15'10" | 17'-11" | 16'-11" | 16'4" |
|  | 14 | 19'-1" | 17 -9" | 17'-2" | 20'0" | 18'7" | 17'-10" |
|  | $16 "$ | 20'-10" | 19'4" | 18'6" | 21'-10" | 20'-3" | 19'-5" |
| PWI 32S, LPI 32Plus | 9-1/2" | 15'-11" | 15'0" | 14'6" | 16'5" | 15'6" | 15'0" |
|  | 11-7/8" | 17'-9" | 16'-9" | 16'3" | 18'7" | 17'-4" | 16'9" |
|  | 14 | 19'-9" | 18'3" | 17'7" | 20'8" | 19'-2" | 18'-4" |
|  | $16 "$ | 21'-5" | 19'-11" | 19'1" | 22'-6" | 20'-10" | 20'0" |
| PWI 36L, LPI 36 | 11-7/8" | 18-4" | $17^{\prime \prime}-2^{\prime \prime}$ | 16'7" | 19'-2' | 17'-9" | 17'-2" |
|  | 14 " | 20'4" | 18-10" | 18'0" | 21'-4" | 19'-9" | 18'-11" |
|  | $16 "$ | 22'-1" | 20'5" | 19'7" | 23'-2" | 21'-5" | 20'6" |
| PWI 42S, LPI 42Plus | 9-1/2" | 17'-0" | 16'0" | 15'5" | 17-7" | 16'6" | $16^{\prime}-0^{\prime \prime}$ |
|  | 11-7/8" | 19'4" | 17-11" | 17'4" | 20'4" | 18'9" | 18'0" |
|  | 14 " | 21'7" | 19'-11" | 19'1" | 22'-7" | 20'-11" | $20^{\prime}-0^{\prime \prime}$ |
|  | $16 "$ | 23'6" | 21'-8" | 20'9" | 24'-8" | 22'-9" | 21'-9" |
| PWI 52S, LPI 52Plus | 11-7/8" | 19'-11" | 18'-5" | 17'-8" | 20'-11" | 19'-4" | 18'6" |
|  | 14 " | 22'-2" | 20'5" | 19'-7" | 23'-3" | 21'-5" | $20^{\prime}-6{ }^{\prime \prime}$ |
|  | $16 "$ | 24'-1" | 22'-3" | 21'-3" | $25^{\prime \prime} 4^{\prime \prime}$ | 23'-4" | $22^{\prime \prime} 4^{\prime \prime}$ |
| PWI 56L, LPI 56 | 11-7/8" | 20'4" | 18'9" | 17'-11" | 21'-4" | 19'-8" | 18'-10" |
|  | 14 " | 22'-7" | 20'-10" | 19'-11" | 23'-8" | 21'-10" | 20'-10" |
|  | $16 "$ | $24^{\prime}-6 "$ | $22^{\prime}-7{ }^{\prime \prime}$ | 21'7" | 25'9" | 23'9" | 22-8" |

## Design Assumptions:

1. The spans listed are the clear distance between supports. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform floor loads only, for standard load duration.
3. These tables reflect the additional stiffness for vibration provided by a 19/32 OSB rated sheathing, or equal, attached as indicated (Nailed Only or Glued \& Nailed) to the top flange.
4. Live load deflection is limited to $\mathrm{L} / 360$ "bare joist."
5. Total load deflection is limited to $\mathrm{L} / 240$.
6. The spans are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing resistance of an SPF wall plate.

# Floor Span Tables: 23/32 OSB Sheathing Specified Floor Loads: 40 PSF Live Load, 15 PSF Dead Load 

## Table Usage:

1. Select the appropriate table based on the floor system construction.
2. Select the Simple Span or Continuous Span section of the table, as required.
3. Find a span that meets or exceeds the required clear span.
4. Read the corresponding joist series, depth and spacing.

Caution: For floor systems that require both simple span and continuous span joists, it is a good idea to check both before selecting a joist. Some conditions are controlled by continuous span rather than simple span.


## 23/32 OSB SHEATHING NAILED ONLY

| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  |  |  | Direct Attached 1/2" Gypsum Ceiling |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  |
|  |  | 12" oc | $16^{\prime \prime}$ oc | 19.2" oc | 24" oc | 12" Oc | $16^{\prime \prime} 00$ | 19.2" oc | 24" oc | 12" Oc | 16" Oc | 19.2" oc | 24" oc | $12^{\prime \prime}$ oc | 16" Oc | 19.2" oc | 24" oc |
| PWI 18S, LPI 18 | 9-1/2 | 14'-2' | 13'-3" | 12'-8" | 12'0" | 14'-8" | 13'8" | 13'1' ${ }^{\prime \prime}$ | 12'-5" | 14'7" | 13'7" | 13'-0" | 12'4" | 15'-1" | 14'-1" | 13'-5" | 12'-9" |
|  | 11-7/8" | 16'-1' | 15'0" | 14'-4" | 13'8" | 16'-8" | $15^{\prime}-6 "$ | 14'-10" | 14'-1' | 16'6" | 15'5" | 14'-9" | 14'0" | 17'-1' | $15^{\prime}-11^{\prime \prime}$ | 15'3" | $14^{\prime}-6{ }^{\prime \prime}$ |
| PWI 20S, LPI 20Plus | 9-1/2" | 15'0" | 14'-0" | 13'-4" | 12'9" | 15'-6" | 14'-5" | 13'-10" | 13'-2" | $15^{\prime}-4^{\prime \prime}$ | 14'-4" | 13'-8" | 13'0" | 15'-11" | $14^{\prime}-10^{\prime \prime}$ | 14'-2" | $13^{\prime}-6{ }^{\prime \prime}$ |
|  | 11-7/8" | 16'-11" | 15'9" | $15^{\prime \prime} 1^{\prime \prime}$ | 14'4" | 17'-6" | $16^{\prime}-4 "$ | $15^{\prime}-7{ }^{\prime \prime}$ | 14'-10" | 17'-4" | 16'-2" | 15'6" | 14'-9" | 18'-1' | 16'9" | $16^{\prime}-0{ }^{\prime \prime}$ | 15'3" |
|  | $14 "$ | 18'-8" | 17'-3" | 16'6" | 15'8" | 19'-7" | 17-11" | 17'-1' | 16'3" | 19'-3" | 17'-8" | 16-11" | 16'1" | 20'3" | 18'6" | 17'-7' | 16'-9" |
|  | $16 "$ | 20'6" | 18-8" | 17'-8" | 16'-10" | 21'-6" | 19'7" | 18'6" | 17'-6" | 21'-2" | 19'-4" | 18'3" | 17'-4" | 22'-2" | $20^{\prime}-4$ " | 19'-3" | 18'-0" |
| PWI 32S,IPI 32Plus | 9-1/2" | 15'7" | 14'-6" | 13'-10" | 13'-2" | 16'-1" | 15'0" | $14^{\prime}-4{ }^{\prime \prime}$ | 13'-8" | 15'-11" | 14'-10" | $14^{\prime}-2{ }^{\prime \prime}$ | 13'-6" | 16'-6" | $15^{\prime \prime} 4^{\prime \prime}$ | $14^{\prime}-8{ }^{\prime \prime}$ | 13'11" |
|  | 11-7/8" | $17^{\prime}-6{ }^{\prime \prime}$ | 16'-4" | $15^{\prime} 7{ }^{\prime \prime}$ | 14'-10" | 18'-3" | 16'-11" | $16^{\prime}-2^{\prime \prime}$ | 15'-4" | 17'-11" | 16'9" | $16^{\prime}-0^{\prime \prime}$ | 15'2" | 18'-10" | $17^{\prime \prime}-4^{\prime \prime}$ | 16'-7' | 15'-9" |
|  | $14{ }^{\prime \prime}$ | 19'-5" | 17'-9" | $17^{\prime}-0^{\prime \prime}$ | 16'-2" | 20'5" | 18'7" | 17-7' | 16-9" | 20'0" | 18'-4" | 17'-5" | 16'7" | 21'-0" | 19'-3" | 18'-2" | 17-2" |
|  | $16^{\prime \prime}$ | 21'-2" | 19'-4" | 18'-3" | $17^{\prime \prime}-4{ }^{\prime \prime}$ | 22'-3" | $20^{\prime \prime} 4^{\prime \prime}$ | 19'-2" | 18'-0" | 21'-10" | 20'0" | 18'-11" | 17'-9" | 22'-11" | 21'-0" | 19'-10" | 18-7" |
| PWI 36L, LPI 36 | 11-7/8" | 18'1" | 16'-10" | $16^{\prime}-1{ }^{\prime \prime}$ | 15'-4" | 19'-0" | 17'-5" | 16'8" | 15'-10" | 18'7" | 17'-2" | 16'5" | 15'-8" | 19'-6" | 17'-10" | 17'-1" | 16'-3" |
|  | 14" | 20'-2" | 18-5" | $17^{\prime \prime}$-6" | 16'-8" | 21-2" | 19'-4" | 18'-3" | 17-3" | 20'9" | 18'-11" | 17'-11" | $17^{-}-0^{\prime \prime}$ | 21-9" | 19'11" | 18'-10" | $17^{\prime}-8{ }^{\prime \prime}$ |
|  | $16{ }^{\prime \prime}$ | 21'-11" | 20'0" | 18'-11" | 17'-9" | 23'-0" | 21'0" | 19'-10" | 18'7" | 22'-7" | 20'8" | 19'-6" | 18'-4" | 23'-8" | 21'-8" | 20'6" | 19'-3" |
| PWI 42S, LPI 42Plus | 9-1/2" | 16'11" | 15'9" | 15'-1" | 14'-4" | 17'-6" | 16'4" | 15-7" | 14'-10" | 17'-3" | 16'-1' | $15^{\prime \prime}-4^{\prime \prime}$ | 14'-7" | 17'-10" | $16^{\prime}-7{ }^{\prime \prime}$ | 15'-11" | 15 '1" |
|  | 11-7/8" | 19'-5" | 17'-9" | $17^{\prime}-0^{\prime \prime}$ | 16'-2" | 20'-4" | 18'7" | 17'-7" | 16'9" | 19'-10" | 18'-2" | $17^{\prime \prime} 4^{\prime \prime}$ | $16^{\prime}$ '6" | 20'-10" | 19'-1" | 18'0" | 17'-1" |
|  | $14^{\prime \prime}$ | 21'-8" | 19'-9" | 18'-8" | 17'-7" | 22'9" | 20'9" | 19'-7" | 18'-4" | $22^{\prime}-2{ }^{\prime \prime}$ | 20'3" | 19'-2" | 18'0" | 23'-4" | 21'-4" | 20'-2" | 18-11" |
|  | $16 "$ | 23'8" | 21'7" | 20'-4" | 19'-1" | 24'-10" | 22'-8" | 21'5" | 20'1' ${ }^{\prime \prime}$ | 24'-3" | 22'-2" | 20'-11" | 19'-8" | 25'6" | 23'-4" | 22'0" | 20'8" |
| PWI 52S, LPI 52Plus | 11-7/8" | 20'0" | 18-4" | 17'-5" | $16^{\prime}-7{ }^{\prime \prime}$ | 21-0" | 19'-2' | 18'-2" | 17'-2' | 20'6" | 18'-9" | 17'9" | 16'-11" | 21'6" | 19'-8" | 18'7" | $17^{\prime \prime}$ '6" |
|  | $14^{\prime \prime}$ | 22'-4" | 20'5" | 19'-3" | 18'-1" | 23'5" | 21'-5" | 20'3" | 19'0" | 22'10" | 20'11" | 19'9" | 18'7" | 24'0" | 21-11" | 20-9" | 19'6" |
|  | $16 "$ | $24^{\prime \prime}-4{ }^{\prime \prime}$ | 22'-3" | $21^{\prime}-0^{\prime \prime}$ | 19'-9" | 25'7" | $23^{\prime}-4^{\prime \prime}$ | 22'-1" | 20'9" | 24'-11" | 22'10" | 21'7" | 20'3" | 26'-2" | 24'-0" | 22'-8" | 21'-3" |
| PWI 56L, LPI 56 | 11-7/8" | 20'6" | 18'8" | 17'-9" | 16'-10" | 21'6" | 19'-8" | 18'7" | 17'6" | 21-0" | 19'-2" | 18'1' ${ }^{\prime \prime}$ | 17'-2" | 22'0" | 20'1' | 19'0" | 17'-10" |
|  | $14^{\prime \prime}$ | 22'-10" | 20'-10" | 19'-8" | 18'5" | 24'0" | 21-10" | 20'-8" | 19'-4" | 23'4" | 21'-4" | 20'-2" | 18-11" | 24'-6" | 22'-5" | 21'-2" | 19'-10" |
|  | 16" | 24'-10" | 22'8" | 21-4" | 20'1' | 26'1" | 23-10" | 22'-6" | 21'-1' | 25'5" | 23'-3" | 21'-11" | 20'7" | 26'-8" | 24'5" | 23'-1' | 21-8" |

23/32 OSB SHEATHING GLUED \& NAILED

| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  |  |  | Direct Attached 1/2" Gypsum Ceiling |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  |
|  |  | 12" oc | 16" oc | 19.2 ${ }^{\text {oc }}$ | 24" OC | 12" Oc | $16^{\prime \prime}$ oc | 19.2" oc | 24" 0 c | 12" Oc | 16" oc | 19.2" oc | 24" oc | 12" Oc | 16" OC | 19.2" oc | 24" 0 C |
| PWI 18S, LPI 18 | 9-1/2" | 15'-8" | 14'-10" | 14'-4" | 13'-2" | 16'2' | 15'-4" | 14'-9" | 13'7" | 16'-2' | 15'-3' | $14^{\prime}-4^{\prime \prime}$ | 13'-2" | 16'8" | 15'9" | $15^{\prime}-2{ }^{\prime \prime}$ | 13'7" |
|  | 11-7/8" | 17'-7" | 16'-7" | 16'0" | $14^{\prime}-10^{\prime \prime}$ | 18'-4" | 17'-2" | $16^{\prime}-7{ }^{\prime \prime}$ | 14'9" | 18-2" | $17^{\prime}-2^{\prime \prime}$ | 16'7" | $14^{\prime}-10^{\prime \prime}$ | 19'-1' | 17'-9" | $16^{\prime}-7{ }^{\prime \prime}$ | 14'-9" |
| PWI 20S, LPI 20Plus | 9-1/2" | 16'-4" | 15'-4" | 14'-10" | 14'-3" | $16^{\prime}-10^{\prime \prime}$ | 15'-11" | $15^{\prime \prime} 4^{\prime \prime}$ | 14'8" | 16'9" | 15'-10" | 15'3' ${ }^{\prime \prime}$ | 14'-5" | $17^{\prime \prime}-4$ | 16'4" | 15'-9" | 15'-2' |
|  | 11-7/8" | 18'-4" | 17'-3" | $16^{\prime}-7{ }^{\prime \prime}$ | 15'-11" | 19'-3" | 17'-10" | 17-2" | 16'6" | 19'-0" | 17'-9" | 17'-1' | $16^{\prime}-5 "$ | 19'11" | 18'6" | 17'-8" | 17'0" |
|  | $14{ }^{\prime \prime}$ | 20'6" | 19'0" | 18'1" | 17'-4" | 21'5" | 19'-11" | 18-11" | 18'0" | 21'-2" | 19'-8" | 18-10" | 17'-10" | 22'3" | 20'8" | 19'-9" | 18-9" |
|  | 16" | 22'-4" | 20'8" | 19'-9" | 18'-9" | 23'-5" | 21'-8" | 20'-8" | 19'7" | 23'-1' | 21'-6" | 20'6" | 19'-6" | 24'-3" | 22'-7" | 21'7" | 20'4" |
| $\begin{aligned} & \text { PWI 32S, } \\ & \text { LPI 32Plus } \end{aligned}$ | 9-1/2" | 16-9" | 15'-10" | 15'-3" | 14-8' ${ }^{\prime \prime}$ | 17-4" | $16^{\prime}-4$ " | 15-9" | 15'1" | 17'-2" | $16^{\prime}-2{ }^{\prime \prime}$ | 15'-8" | 15'0" | 17'-9" | 16'9" | $16^{\prime}-2{ }^{\prime \prime}$ | 15'6" |
|  | 11-7/8" | 19'-0" | 17'-8" | 17'-1" | 16'-4" | 19'11" | 18'6" | 17'-8" | 16'11" | 19'7" | 18'-3" | 17'-6" | 16'-10" | 20'7" | 19'-1" | 18'3" | 17'-5" |
|  | 14 " | 21'1' | 19'7" | 18'8" | 17'-9" | 22'-2" | 20'6" | 19'-7" | 18'7" | 21-10" | 20'3" | 19'-4" | 18'-4" | 22-10" | 21'-3" | 20'3" | 19'3" |
|  | 16 " | 23'-0" | 21'-3" | 20'-3" | 19'-3" | 24'-1' | 22'-4" | 21'-3" | 20'-2" | 23'-9" | 22'0" | 21'-0" | 19'-8" | 24'11" | 23'-2" | 22'-1" | 20'4" |
| $\begin{gathered} \text { PWI 36L, } \\ \text { LPI } 36 \end{gathered}$ | 11-7/8" | 19'-7" | 18'2" | 17'-5" | 16'9" | 20'7" | 19'0" | 18'-2" | 17'-4" | 20'2" | 18-9" | 17'-10" | 17'-2" | 21'2" | 19'-8" | 18-9" | 17'-9" |
|  | $14^{\prime \prime}$ | 21'9" | 20'1" | 19'-2" | 18-2" | 22'-10" | 21'1" | 20'1' | 19'1" | 22'5" | 20'9" | 19'10" | 18-10" | 23'6" | 21'10" | 20'10" | 19'9" |
|  | 16" | 23'7" | 21-10" | 20'-10" | 19'9" | 24'-9" | 22-11" | 21'-10" | 19'9" | $24^{\prime}-4{ }^{\prime \prime}$ | 22'-7" | 21'6" | 20'5" | 25'6" | 23'9" | 22'-7" | 19'9" |
| PWI 42S, LPI 42Plus | 9-1/2" | 17-11" | 16-10" | 16'3" | 15'7" | 18'9" | 17'-5" | 16'9" | 16'-1' | 18-4" | 17'-2" | 16'7" | 15'-10" | 19'-3" | 17'-10" | 17'-2" | 16'5" |
|  | 11-7/8" | 20-9" | 19'-2" | 18'3" | 17'-5" | 21'9" | 20'-1" | 19'-1" | 18'1" | 21'3" | 19'-8" | 18'-9" | 17'-10" | 22'-4" | 20'8" | 19'-8" | 18'-8" |
|  | 14 " | 23'0" | 21'3" | 20'3" | 19'2" | 24'-2" | 22'-4" | 21'-3" | 20'2" | 23'8" | 21-11" | 20'-10" | 19'9" | 24-10" | 23'-0" | 21'-11" | 20'9" |
|  | 16" | 25'1' | 23-2" | 22'1" | 20'11" | 26'4" | 24'-4" | 23'-2" | 21'11" | 25'9" | 23-10" | 22'-9" | 21'6" | 27-1" | 25'-1' | 23'11" | 22'-7" |
| PWI 52S,LPI 52Plus | 11-7/8" | 21'3" | 19'8" | 18-9" | 17'-10" | 22'4" | 20'7" | 19'-8" | 18'7" | 21-9" | 20'2" | 19'-3" | 18-3" | 22'-10" | 21'-2" | 20'2" | 19'-1" |
|  | 14" | 23'8" | 21-10" | 20'9" | 19'8" | 24'-10" | 22'-11" | 21'-10" | 20'8" | 24'-2" | 22'-5" | 21-4" | 20'3" | 25'5" | 23-6" | 22'-5" | 21'3" |
|  | $16 "$ | 25'9" | 23'9" | 22'-7" | 21'-5" | 27'0" | 24-11" | 23'9" | 22'6" | 26'4" | 24'-5" | 23'3" | 22'0" | 27'-8" | 25'-8" | 24'-5" | 23'-1' |
| PWI 56L, LPI 56 | 11-7/8" | 21'9" | 20'1" | 19'1" | 18'-1" | 22'-10" | 21'0" | 20'-0" | 18'11" | 22'3" | 20'7" | 19'-7" | 18'6" | 23'-4" | 21'7" | 20'6" | 19'-5" |
|  | 14" | 24'-1' | 22'-3" | 21'-2" | 20'-0" | 25'-4" | $23^{\prime \prime} 4^{\prime \prime}$ | 22'-2" | 21'0" | 24'-8" | 22-10" | 21'-8" | 20'6" | 25'-11" | 23'-11" | 22'-10" | 21'7" |
|  | $16 "$ | 26'-2" | $24^{\prime}-2{ }^{\prime \prime}$ | 22'-11" | 21'-9" | 27'-6" | $25^{\prime}-4 \prime$ | 24'-1' | 22'-10" | 26'-9" | 24-9" | 23'-7" | $22^{\prime}-4 \prime$ | 28-2" | 26'1" | 24'9" | 23'5" |

## Design Assumptions:

1. The spans listed are the clear distance between supports. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform floor loads only, for standard load duration.
3. These tables reflect the additional stiffness for vibration provided by a $23 / 32$ OSB rated sheathing, or equal, attached as indicated (Nailed Only or Glued \& Nailed) to the top flange.
4. Live load deflection is limited to $\mathrm{L} / 360$ "bare joist."
5. Total load deflection is limited to $\mathrm{L} / 240$.
6. The spans are based on an end bearing length of at least $1-3 / 4^{\prime \prime}$ and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing resistance of an SPF wall plate.

## Additional Notes

1. These spans have been designed to meet the Limit States Design and vibration requirements of the National Building Code of Canada.
2. Web stiffeners are not required for any of the spans in these tables.
3. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange.
4. For conditions not shown, use the Uniform Floor Load (PLF) tables, use the Exacte by PWT software or contact your PWT" distributor for assistance.

# Floor Span Tables: 5/8 OSB Sheathing Specified Floor Loads: 40 PSF Live Load, 15 PSF Dead Load 

## Table Usage:

1. Select the appropriate table based on the floor system construction.
2. Select the Simple Span or Continuous Span section of the table, as required.
3. Find a span that meets or exceeds the required clear span. 4. Read the corresponding joist series, depth and spacing Caution: For floor systems that require both simple span and continuous span joists, it is a good idea to check both before selecting a joist. Some conditions are controlled by continuous span rather than simple span.


## 5/8 OSB SHEATHING NAILED ONLY

| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  | Direct Attached 1/2" Gypsum Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  | Maximum Continuous Spans |  |  | Maximum Simple Spans |  |  | Maximum Continuous Spans |  |  |
|  |  | 12" Oc | $16^{\prime \prime} 00$ | 19.2" oc | 12" Oc | 16" Oc | 19.2" oc | 12" OC | 16 Coc | 19.2" oc | 12" oc | $16^{\prime \prime} 00$ | 19.2" oc |
| PWI 18S, LPI 18 | 9-1/2" | 13'-9" | 12'-9" | 12'3" | 14'-2" | 13'-2" | 12'8" | 14'1' ${ }^{\prime \prime}$ | 13'-2' | 12'-7" | 14'7" | 13'7" | 13'0" |
|  | 11-7/8" | 15'6" | $14^{\prime}$ '6" | 13'-11" | 16'1" | 15'0" | $14^{\prime}-4 "$ | 16'0" | 14'-11" | $14^{\prime}-4{ }^{\prime \prime}$ | $16^{\prime}-7{ }^{\prime \prime}$ | 15'-5" | 14'-10" |
| PWI 20S, LPI 20Plus | 9-1/2" | $14^{\prime}-6{ }^{\prime \prime}$ | 13'6" | 12'-11" | 15'0" | 13'-11" | 13'-4" | 14'-11" | 13'-10" | 13'-3" | $15^{\prime}-5{ }^{\prime \prime}$ | 14'4" | 13'9" |
|  | 11-7/8" | 16'4" | 15'-3" | 14'-7" | 16'-11" | 15'9" | 15'1" | 16'-10" | 15-8" | 15'0" | 17'-5" | 16'-3" | $15^{\prime}-7{ }^{\prime \prime}$ |
|  | 14 " | 17'-11" | 16'-8" | 16'0" | 18'9" | 17'-3" | 16'6" | 18'6" | 17'-2" | 16'5" | 19'-5" | 17-9" | $17^{-0 "}$ |
|  | $16 "$ | 19'-7" | 17-11" | $17^{\prime}-2{ }^{\prime \prime}$ | 20'7" | 18'9" | 17'-9" | 20'-4" | 18'-7' | 17'-8" | 21'-4" | 19'6" | 18'6" |
| PWI 32S, LPI 32Plus | 9-1/2" | 15'-1" | 14'0" | 13'-5" | 15'7" | 14'-6" | 13'-11" | 15'5" | 14'-4" | 13'-9" | $16^{\prime}-0^{\prime \prime}$ | 14'-10" | $14^{\prime}-3 "$ |
|  | 11-7/8" | 16'11" | 15'9" | $15^{\prime \prime} 1^{\prime \prime}$ | 17'-6" | $16^{\prime}-4{ }^{\prime \prime}$ | 15'-8" | $17^{\prime}-4^{\prime \prime}$ | 16'-2" | $15^{\prime}-6{ }^{\prime \prime}$ | 18'-1' | 16'9" | $16^{\prime}-1{ }^{\prime \prime}$ |
|  | $14{ }^{\prime \prime}$ | 18'-7" | $17^{\prime \prime}-2^{\prime \prime}$ | 16'5" | 19'-6" | 17'-10" | 17'-1" | 19'3" | 17-8" | 16'11" | 20'2' | 18'5" | $17^{\prime \prime}$-6" |
|  | $16^{\prime \prime}$ | 20'-3" | $18^{\prime}-6 "$ | 17'-7" | 21'-3" | 19'-5" | 18'-5" | 21'0" | 19'-2" | 18'-2" | 22'0" | 20'-2" | 19'1" |
| PWI 36L, LPI 36 | 11-7/8" | $17^{\prime \prime}-5{ }^{\prime \prime}$ | $16^{\prime}-3 "$ | 15'7" | 18'-2" | 16'-10" | 16'-1" | 17'-10" | 16'8" | 15'-11" | 18'9" | 17'-3" | $16^{\prime}$-6" |
|  | $14^{\prime \prime}$ | 19'-3" | $17^{\prime \prime}$ " ${ }^{\prime \prime}$ | 16'-11' | 20'3" | 18'6" | 17'-7" | 19'-11" | 18'-2" | 17-4" | 20'11" | 19'-1" | 18'1" |
|  | $16 "$ | $21^{\prime}-0^{\prime \prime}$ | $19^{\prime}-2{ }^{\prime \prime}$ | 18'2" | 22'-0" | 20'1" | 19'-1' | 21'8' | 19'-10" | 18'-9" | 22'-9" | 20'10" | 19'-9" |
| PWI 42S, LPI 42Plus | 9-1/2" | 16'4" | $15^{\prime}-2{ }^{\prime \prime}$ | 14'7' ${ }^{\prime \prime}$ | 16'-11" | 15'9" | 15'-1" | $16^{\prime}-8$ " | 15'7" | 14'-11" | 17'-3" | 16'1" | 15'-5" |
|  | 11-7/8" | 18'7" | 17-2" | 16'5" | 19'6" | 17'-9" | $17^{\prime}-0 "$ | 19'-1' | 17'-6" | 16'10" | 20'-0" | 18'3" | 17'-5" |
|  | $14^{\prime \prime}$ | 20'-8" | 18-11" | 17'-11" | 21'-9" | 19'-10" | 18'-10" | 21'-3' | 19'-5" | 18'-5" | 22'-4" | 20'5" | 19'-4" |
|  | $16 "$ | 22'-7" | 20'8" | 19'6" | 23'9" | 21'-8" | $20^{\prime}-6 "$ | 23'3" | 21'-3" | 20'-2" | 24'6" | 22'4" | 21'-2" |
| PWI 52S, LPI 52Plus | 11-7/8" | 19'-2" | 17'-7" | 16'-11" | 20'-1" | 18'4'4' | 17'-6" | 19'-8" | 18'0" | 17'-3" | 20'-8" | 18-11" | 17'-11" |
|  | $14^{\prime \prime}$ | 21'-4" | 19'6" | 18'6" | 22'-5" | 20'6" | 19'-5" | 21'-11" | 20'-1" | 19'-0" | 23'-0" | 21'1" | 20'0" |
|  | $16 "$ | $23^{\prime}-4{ }^{\prime \prime}$ | 21'3" | 20'2" | 24'-6" | 22'4" | $21^{\prime \prime}-2^{\prime \prime}$ | 23'-11' | 21'-11" | 20'-9" | 25'-2" | 23'0" | 21'-10" |
| $\begin{aligned} & \text { PWI 56L, } \\ & \text { LPI } 56 \end{aligned}$ | 11-7/8" | 19'-7" | 17-11" | 17-2" | 20'7" | 18'9" | 17'-10" | 20'1" | 18'-4" | 17'-6" | 21'2" | 19'-4" | 18'3" |
|  | 14" | 21'10" | 19'11" | 18'-10" | 22'-11" | 20'-11" | 19'-10" | 22'5" | 20'5" | 19'-4" | 23'-6" | 21'6" | 20'4" |
|  | $16 "$ | 23-9" | 21'8" | 20'6" | 25'0" | 22'-9" | 21'7" | 24-5" | 22'-3" | 21'-1' | 25-8" | 23'5" | 22'-2" |

5/8 OSB SHEATHING GLUED \& NAILED

| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  | Maximum Continuous Spans |  |  |
|  |  | 12" OC | 16 CO | 19.2" oc | 12" oc | 16" Oc | 19.2" oc |
| PWI 18S, LPI 18 | 9-1/2" | 15'0" | 14'3" | 13'-9" | 15'6" | 14'-8" | 14'-2" |
|  | 11-7/8" | 16'-11" | 16'0" | 15'5" | $17^{\prime \prime}$ " ${ }^{\prime \prime}$ | $16^{\prime}-6{ }^{\prime \prime}$ | 16'0" |
| PWI 20S, LPI 20Plus | 9-1/2" | 15'-8" | 14'9" | 14'-3" | 16'2" | 15'-3" | 14'-9" |
|  | 11-7/8" | 17'-7" | 16'7" | $16^{\prime}-0^{\prime \prime}$ | 18-3" | 17'-2" | 16'7" |
|  | 14 " | 19'-6" | 18-1" | 17'-5" | 20'5" | 18'-11" | 18'1" |
|  | 16 " | 21'-3" | 19'-8" | 18'-10" | 22'-3" | 20'-8" | 19'-9" |
| PWI 32S, LPI 32Plus | 9-1/2" | $16^{\prime}-1{ }^{\prime \prime}$ | $15^{\prime \prime} 2^{\prime \prime}$ | 14'-8" | 16'8" | 15'-8" | 15'-2" |
|  | 11-7/8" | 18'-1" | $17^{\prime}-0{ }^{\prime \prime}$ | 16'5" | 18'11" | 17'-7" | 17'0" |
|  | $14 "$ | 20'1" | 18'7" | 17'-10" | 21'1" | 19'-6" | 18'8" |
|  | 16 " | 21'-10" | $20^{\prime}-3^{\prime \prime}$ | 19'-4" | 22'-11" | 21-3" | 20'-3" |
| PWI 36L, LPI 36 | 11-7/8" | 18-8" | 17'-5" | 16'10" | 19'7" | 18'1" | 17'-5" |
|  | 14 | 20'-8" | 19'-2" | 18'-4" | 21'-8" | 20'-1' | 19'2" |
|  | $16 "$ | $22^{\prime}-6 "$ | 20'-10" | 19'-11" | 23'7" | 21'10" | 20'10" |
| PWI 42S, LPI 42Plus | 9-1/2" | 17'-3" | 16'2" | 15'-8" | 17'-10" | 16'-9" | 16'-2" |
|  | 11-7/8" | 19'-9" | 18-3" | 17'-6" | 20'8" | 19'-1" | 18'-3" |
|  | $14 "$ | 21-11" | 20'3" | 19'-4" | 23'-0" | 21'-3" | 20'-4" |
|  | $16 "$ | 23'11" | 22'-1" | 21'1" | 25'1' ${ }^{\prime \prime}$ | 23'-2" | 22'-1" |
| PWI 52S, LPI 52Plus | 11-7/8" | 20'3" | 18'9" | 17'-11" | 21'-3" | 19'-8" | 18'9" |
|  | 14 " | 22'6" | 20'10" | 19'-10" | 23'-8" | 21'10" | 20'-10" |
|  | $16 "$ | 24'-6" | 22'8" | 21'-7" | 25'-9" | 23'-9" | 22'-8" |
| PWI 56L, LPI 56 | 11-7/8" | 20'8" | 19'1" | 18'-3" | 21'-9" | 20'0" | 19'-1" |
|  | $14^{\prime \prime}$ | 22'11" | 21'-2" | 20'-2" | 24'1' | 22'-3" | 21-2" |
|  | $16 "$ | 24'-11" | 23'0" | 21'-11" | 26'3" | 24'-2" | 23'0" |

## Design Assumptions:

1. The spans listed are the clear distance between supports. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform floor loads only, for standard load duration.
3. These tables reflect the additional stiffness for vibration provided by a $5 / 8$ OSB rated sheathing, or equal, attached as indicated (Nailed Only or Glued \& Nailed) to the top flange.
4. Live load deflection is limited to $\mathrm{L} / 360$ "bare joist."
5. Total load deflection is limited to $\mathrm{L} / 240$.

| Direct Attached 1/2" Gypsum Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Simple Spans |  |  | Maximum Continuous Spans |  |  |
| 12" oc | $16^{\prime \prime}$ Oc | 19.2" oc | 12" oc | $16^{\prime \prime}$ oc | 19.2" oc |
| $15^{\prime \prime} 6^{\prime \prime}$ | 14-8" | $14^{\prime}-2^{\prime \prime}$ | $16^{\prime} 0^{\prime \prime}$ | $15 \cdot 2$ ' | $14^{\prime}-8{ }^{\prime \prime}$ |
| 17'5" | $16^{\prime} 66^{\prime \prime}$ | 16'0" | 18'2" | 17'-1" | $16^{\prime}-6{ }^{\prime \prime}$ |
| 16'1" | 15'2" | 14'-8" | 16'8" | 15'9" | $15{ }^{\prime}-2{ }^{\prime \prime}$ |
| 18'1" | 17-1" | $16^{\prime}-6{ }^{\prime \prime}$ | 19'0" | 17'-8" | 17'-1" |
| 20'2' | 18-9" | 18'00' | 21-2" | 19'8" | 18-10" |
| $22^{\prime \prime} 1^{\prime \prime}$ | 20'6" | 19'-7" | 23-2" | 21'6" | 20'-7" |
| $16^{\prime} 6^{\prime \prime}$ | 15'7" | $15^{5}-1{ }^{\prime \prime}$ | 17-1" | 16'2" | $15 \cdot 7{ }^{\prime \prime}$ |
| 18'-8" | 17'-6" | 16'11" | 19'7" | 18'3" | $17^{\prime}-6{ }^{\prime \prime}$ |
| 20'10" | 19'4" | 18'6" | 21'-10" | 20'3" | 19'5" |
| 22'-8" | 21-0" | 20'10 | 23'9" | 22'-1" | 21'-1" |
| 19'3" | 17'-10" | 17'-3" | 20'2" | 18'9" | 17'-11" |
| 21-4" | 19'10" | 18'11" | 22'5" | 20'10" | 19'11" |
| 23'3" | 21'7" | $20^{\prime} \cdot 7{ }^{\prime \prime}$ | 24'5" | 22'-8" | 21'-8" |
| 17'7" | 16'7" | 16'0" | 18'4" | 17'-2" | $16^{\prime}-7{ }^{\prime \prime}$ |
| 20'4" | 18'9" | 17'-11" | 21'4" | 19'9" | 18-10" |
| 22'-7" | 20-11" | 19'11" | 23'9" | 21-11" | 21-0" |
| 24-7" | 22-9" | 21-9" | 25'10" | 23-11" | 22'-10" |
| 20'10" | 19-3" | 18'-5" | 21'-10" | 20'3" | 19'-4" |
| 23-2" | 21'5" | 20'5" | 24-4" | 22'6" | 21'6" |
| 25'2" | 23'4" | 22'-3" | $26^{\prime} 6{ }^{\prime \prime}$ | 24'6" | 23'-5" |
| 21-3" | 19'7" | 18-9" | 22'3" | 20'7" | 19'-8" |
| 23'7" | 21'-9" | 20'9" | 24'9" | 22'-11" | 21'-10" |
| 25'7" | 23-8" | 22'-7" | 26'11" | 24-11" | 23-9" |

## Additional Notes:

1 These spans have been designed to meet the Limit States Design and vibration requirements of the National Building Code of Canada.
2. Web stiffeners are not required for any of the spans in these tables.
3. Web fillers are required for $1-$-Joists seated in hangers that do not laterally support the top flange.
4. For conditions not shown, use the Uniform Floor Load (PLF) tables, use the Exacte by PWT software or contact your PWT"' distributor for assistance.

# Floor Span Tables: 3/4 OSB Sheathing Specified Floor Loads: 40 PSF Live Load, 15 PSF Dead Load 

## Table Usage:

1. Select the appropriate table based on the floor system construction.
2. Select the Simple Span or Continuous Span section of the table, as required.
3. Find a span that meets or exceeds the required clear span.
4. Read the corresponding joist series, depth and spacing.

Caution: For floor systems that require both simple span and continuous span joists, it is a good
idea to check both before selecting a joist. Some conditions are controlled by continuous span rather than simple span.

## 3/4 OSB SHEATHING NAILED ONLY



| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  |  |  | Direct Attached 1/2" Gypsum Ceiling |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  |
|  |  | 12" OC | $16^{\prime \prime}$ oc | 19.2" OC | 24" OC | 12" OC | 16 " oc | 19.2" oc | 24"0C | 12" OC | 16" Oc | 19.2" oc | 24" OC | 12" Oc | 16 Coc | 19.2" oc | 24" OC |
| PWI 18S, LPI 18 | 9-1/2" | 14'-4" | $13^{\prime}-4{ }^{\prime \prime}$ | 12'-9" | 12'-2' | 14'-10" | 13'10" | 13'-2" | 12'6" | 14'-9" | 13'9" | $13^{\prime}-2$ " | $12^{\prime}-6{ }^{\prime \prime}$ | 15'3' ${ }^{\prime \prime}$ | $14^{\prime}-2^{\prime \prime}$ | 13'7" | 12'-11" |
|  | 11-7/8" | 16'3' ${ }^{\prime \prime}$ | 15'-2" | 14'-6" | 13'9" | 16'-10" | $15 ' 8$ " | 15'0" | 14'3" | 16'-8" | 15'7" | 14'-11" | $14^{\prime}-2^{\prime \prime}$ | 17'-3" | 16'-1' | 15'5" | 14'-8" |
| PWI 20S, LPI 20Plus | 9-1/2" | $15^{\prime}-2^{\prime \prime}$ | 14'-2" | $13^{\prime}-6{ }^{\prime \prime}$ | 12'-10" | 15'-8" | 14'-7" | 13'-11" | 13'3" | 15'-6" | $14^{\prime}-6{ }^{\prime \prime}$ | 13'-10" | 13'2' ${ }^{\prime \prime}$ | 16'1' | 15'0" | $14^{\prime}-4^{\prime \prime}$ | $13^{\prime} 7^{\prime \prime}$ |
|  | 11-7/8" | 17'-1' | 15'-11" | 15'-3" | 14'6" | 17'-9" | $16^{\prime}$ '6" | 15'9" | 15'0" | 17'-6" | 16'4" | $15^{\prime \prime} 8^{\prime \prime}$ | 14'-10" | 18'3" | 16'-11" | $16^{\prime}-2^{\prime \prime}$ | 15'5" |
|  | $14^{\prime \prime}$ | 18'-11" | 17'-5" | 16'-8" | 15'-10" | 19'-10" | 18-2" | 17'-3" | 16'-5" | 19'-6" | 17'-11" | 17'-1' | $16^{\prime}-3 "$ | 20'6" | 18-9" | 17'-9" | $16^{\prime}-10^{\prime \prime}$ |
|  | 16" | 20'9" | 18-11" | 17'-11" | 17'0" | 21'-9" | 19'-11" | 18'9" | 17'7" | 21'5" | 19'-7" | 18'6" | $17^{\prime}-6{ }^{\prime \prime}$ | 22'6" | 20'7" | 19'-5" | 18'-3" |
| PWI 32S,LPI 32Plus | 9-1/2" | 15'-9" | 14'-8" | 14'-0" | 13'-4" | 16'3" | 15'2" | 14'-6" | 13'9" | 16'-1' | 15'0" | 14'-4" | 13'7" | 16'8' | 15'6" | 14'-10" | $14^{\prime}-1{ }^{\prime \prime}$ |
|  | 11-7/8" | $17^{\prime}-9{ }^{\prime \prime}$ | $16^{\prime}$ '6" | $15^{\prime}-9$ " | 15'0" | 18'-6" | 17'-1" | $16^{\prime}-4^{\prime \prime}$ | 15'6" | 18'-2" | 16'-11" | $16^{\prime}-2{ }^{\prime \prime}$ | 15'-4" | 19'1" | $17^{\prime}-6{ }^{\prime \prime}$ | $16^{\prime}-9$ " | 15'-11" |
|  | $14^{\prime \prime}$ | 19'-8" | 18'0" | 17'-2" | 16'-4" | 20'-8' | 18'-10" | 17'-10" | 16'-11" | 20'3" | 18'-6" | $17^{\prime}-7{ }^{\prime \prime}$ | 16'9" | 21'3" | 19'-6" | 18'-5" | 17'-4" |
|  | $16 "$ | 21'6" | 19'7" | 18'6" | 17'-5" | 22'-7" | 20'7" | 19'5" | 18'2' ${ }^{\prime \prime}$ | 22'-1" | 20'-3" | 19'-1' | 17-11" | 23'3" | 21'-3" | 20'-1" | 18-10" |
| PWI 36L, LPI 36 | 11-7/8" | $18^{\prime}-4{ }^{\prime \prime}$ | 17'-0" | $16^{\prime}-3^{\prime \prime}$ | 15'-5" | 19'-3" | $17^{\prime}-7{ }^{\prime \prime}$ | $16^{\prime}-10^{\prime \prime}$ | 16'0'0' | 18'-10" | 17-4" | 16'7" | 15'-9" | 19'9" | 18'-1" | 17'-3" | $16^{\prime}-4{ }^{\prime \prime}$ |
|  | 14" | 20'-5" | 18'8" | $17^{\prime}-8^{\prime \prime}$ | 16-9" | 21'5" | 19'7" | 18'-6" | 17'-5" | 21-0" | 19'-2" | 18'-1' | $17^{\prime}-2{ }^{\prime \prime}$ | 22'0" | 20'2" | 19'-0" | $17^{\prime}-10^{\prime \prime}$ |
|  | $16 "$ | 22'-3" | 20'3" | $19^{\prime}-2^{\prime \prime}$ | 17'-11" | $23^{\prime \prime} 4^{\prime \prime}$ | 21'-4" | $20^{\prime}-1{ }^{\prime \prime}$ | 18'-10" | 22'-10" | 20'-11" | 19'-9" | 18'6" | $24^{\prime}-0^{\prime \prime}$ | 22'0" | 20'9" | 19'5" |
| PWI 42S, LPI 42Plus | 9-1/2" | $17^{\prime \prime} 1^{\prime \prime}$ | 15'-11" | $15^{\prime \prime} 3^{\prime \prime}$ | 14'-5" | 17'-8" | $16^{\prime}$ '6" | 15'-9" | 14'-11" | 17'-5" | $16^{\prime}-3^{\prime \prime}$ | $15^{\prime}-6{ }^{\prime \prime}$ | 14'-9" | 18'1" | 16'-11" | $16^{\prime}-1{ }^{\prime \prime}$ | 15'-3" |
|  | 11-7/8" | 19'-8" | 17-11" | 17'-2" | $16^{\prime}-3 "$ | 20'-7" | 18'-10" | 17'-9" | 16'11" | 20'1" | 18'5" | $17^{\prime \prime}$-6 | $16^{\prime}-7{ }^{\prime \prime}$ | 21'1" | 19'4" | 18-3" | $17^{\prime \prime}-3 "$ |
|  | 14 " | 21-11" | 20'0" | 18'-11" | 17'-9" | 23'-0" | 21'0" | 19'-10" | 18'7" | 22'5" | 20'6" | 19'-5" | 18-2" | 23'7" | 21-7" | 20'-5" | 19'1" |
|  | $16 "$ | 24'0" | 21'-10" | 20'-8" | 19'-4" | 25'2" | 23'0" | 21'-8" | $20^{\prime}-4{ }^{\prime \prime}$ | 24'6" | 22'5" | 21'-2" | 19'-10" | 25-10" | 23'7" | 22'-4" | 20'11" |
| PWI 52S, LPI 52Plus | 11-7/8" | 20'4" | 18'7" | 17'-7' | 16'-9" | 21'4" | 19'-5" | 18'-5" | $17^{\prime \prime} \mathbf{4}^{\prime \prime}$ | 20'9" | 19'-0" | 17'-11" | 17'-1" | 21'9" | 19'-11" | 18'-10" | 17'-8" |
|  | 14" | 22'-7" | 20'-8" | 19'6" | 18'-4" | 23'-9" | 21'-8" | 20'6" | 19'-2" | 23'1" | 21'-2" | 20'0" | 18'9" | 24'-3" | 22'3" | 21'0" | 19'-8" |
|  | $16 "$ | 24'-8" | 22'6" | 21'-3" | 19'-11" | 25'-11" | 23'-8" | $22^{\prime}-4{ }^{\prime \prime}$ | 20'-11" | 25'3" | 23'1' | 21'-10" | 20'6" | 26'6" | 24'-3" | 23'0" | 21'6" |
| PWI 56L, LPI 56 | 11-7/8" | 20'9" | 19'0" | 17'-11" | 17'-0" | 21'10" | 19'-11" | 18'-10" | 17'-8" | 21'-3" | 19'-5" | 18'-4" | 17'-4" | $22^{\prime}-4{ }^{\prime \prime}$ | 20'5" | 19'-3' | 18'-0" |
|  | 14" | 23'-1" | 21'1' | 19'11" | 18'8" | 24'-3" | 22'-2" | 20'-11" | 19'7" | 23'-7" | 21'7" | 20'5" | 19'-1' | 24-10" | 22'-8" | 21'-5" | 20'-1' |
|  | $16 "$ | $25^{\prime}-2{ }^{\prime \prime}$ | 22-11" | 21-8" | 20'3" | 26'5" | 24'-2" | 22'-9" | 21'4" | 25'-8" | 23'6" | 22'-3" | 20'10" | 27'0" | 24'-9" | 23-4" | 21-11" |

3/4 OSB SHEATHING GLUED \& NAILED

| Series | Depth | No Direct Attached Ceiling |  |  |  |  |  |  |  | Direct Attached 1/2" Gypsum Ceiling |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  | Maximum Simple Spans |  |  |  | Maximum Continuous Spans |  |  |  |
|  |  | 12" oc | 16" Oc | 19.2" OC | 24" oc | $12^{\prime \prime} 00$ | 16 CO | 19.2" OC | 24"0C | 12" OC | 16" OC | $19.2{ }^{\text {" oc }}$ | 24" 0 | 12" oc | $16^{\prime \prime}$ oc | 19.2" OC | 24" 0 C |
| PWI 18S, LPI 18 | 9-1/2" | 15'-10" | 15'0" | $14^{\prime \prime} 4^{\prime \prime}$ | 13'2" | 16'5" | 15'6" | 14'11" | 13'7" | 16'4" | 15'-3" | $14^{\prime \prime} 4^{\prime \prime}$ | 13'2' | 16'-11" | 16'0" | 15'-2" | 13'7" |
|  | 11-7/8" | 17'-10" | 16'-10" | $16^{\prime}-3 "$ | $14^{\prime}-10^{\prime \prime}$ | 18'7" | 17'-5" | $16^{\prime}-7{ }^{\prime \prime}$ | 14'-9" | 18'5" | $17^{\prime}-4{ }^{\prime \prime}$ | $16^{\prime}-8^{\prime \prime}$ | $14^{\prime}-10^{\prime \prime}$ | 19'-4" | 18'0" | $16^{\prime}-7{ }^{\prime \prime}$ | 14'-9" |
| PWI 20S, LPI 20Plus | 9-1/2" | 16'6" | $15{ }^{\prime \prime} \mathbf{7}^{\prime \prime}$ | 15'0" | 14'-5" | 17'-1" | 16'-1" | 15'6" | 14'-10" | 16'-11" | 16'0" | 15'-5" | 14'-5" | 17'-6" | 16'6" | 15'-11" | 15'-2' |
|  | 11-7/8" | 18'8" | 17'-5" | 16'-10" | $16^{\prime}-1{ }^{\prime \prime}$ | 19'6" | 18'-1' | 17'-5" | 16'8" | 19'-3" | 17'-11" | 17'-3' | $16^{\prime} 7{ }^{\prime \prime}$ | 20'3" | 18'-10" | 17'-11" | 17'-2' |
|  | 14 | 20'9" | 19'-3" | 18'-4" | $17^{\prime \prime}$ '6" | 21'-9" | 20'-2" | 19'-3" | 18'-3" | 21'6" | 20'0" | 19'-1" | 18'1" | 22'-7" | 21'0" | 20'0" | 19'0" |
|  | 16" | 22'-8" | 21'0" | 20'0" | 19'0" | 23'9" | 22'-0" | 21'0" | 19'-10" | 23'-5" | 21'-10" | 20'10" | 19'8" | 24'7" | 22'11" | 21'-10" | 20'4" |
| $\begin{aligned} & \text { PWI 32S, } \\ & \text { LPI 32Plus } \end{aligned}$ | 9-1/2" | $17^{\prime}-01$ | $16^{\prime}-0{ }^{\prime \prime}$ | 15'-5" | 14'9" | 17-7" | $16^{\prime}-7{ }^{\prime \prime}$ | 15'-11" | $15^{\prime}-3$ " | 17'-5" | 16'5" | 15'-10" | 15'2" | 18'1" | $17^{\prime}-0^{\prime \prime}$ | $16^{\prime}-4$ " | 15'8" |
|  | 11-7/8" | 19'-4" | 17-11" | 17'-3" | $16^{\prime}$ '6" | 20'3" | 18'-9" | 17'-10" | 17'-1" | 19'-11" | 18'6" | $17^{\prime}-8{ }^{\prime \prime}$ | 17'-0" | 20'-10" | 19'-5" | 18'6" | 17'-7" |
|  | 14 | 21'5" | 19'-10" | 18'-11" | 17'-11" | 22'-6" | 20'-10" | 19'-10" | 18'9" | 22'-1" | 20'6" | 19'-7" | 18'7" | 23'2" | 21'-7" | 20'7" | 19'5" |
|  | $16 "$ | 23'4" | 21'-7" | 20'7" | 19'-6" | $24^{\prime}-6{ }^{\prime \prime}$ | 22'-8" | 21'7" | 20'4" | 24'-1" | $22^{\prime}-4$ | 21'-4" | 19'8" | 25'3" | 23'6" | 22'-5" | 20'-4" |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 19'11" | 18'5" | 17'-8" | 16'-11" | 20'-10" | 19'-4" | 18'-5" | 17'-6" | 20'6" | 19'0" | 18'-1' | 17-4" | 21'6" | 19'-11" | 19'0" | 18'0" |
|  | 14" | 22'-1" | 20'5" | 19'-6" | 18'5" | 23'-2" | 21'-5" | 20'5" | 19'4" | 22'-8" | 21'1" | 20'-1' | 19'0" | 23'-10" | 22'1" | 21'1" | 19'9" |
|  | $16 "$ | 24'0" | 22'-2" | 21'1" | 20'0" | 25'2" | 23'-3" | 22'-2" | 19'9" | 24'-8" | 22-11" | 21-10" | 20'8" | 25'-11" | 24'-1" | 22'-11" | 19'9" |
| PWI 42S, LPI 42Plus | 9-1/2" | 18'2" | $17^{\prime \prime}-1{ }^{\prime \prime}$ | 16'-5" | 15'9" | 19'-1' | 17'-8" | $17^{\prime}-0{ }^{\prime \prime}$ | 16'3" | 18'7" | 17'-5" | 16'-9" | 16'0" | 19'-6" | 18-1" | 17'-4" | $16^{\prime} 7{ }^{\prime \prime}$ |
|  | 11-7/8" | 21'0" | 19'-5" | 18'6" | 17'-7" | 22'-1" | 20'5" | 19'-5" | 18-4" | 21'7" | 20'0" | 19'0" | 18'0" | 22'-7" | 20'-11" | 19'-11" | 18'-11" |
|  | $14^{\prime \prime}$ | 23'5" | 21-7" | 20'7" | 19'-5" | 24'-6" | 22'-8" | 21-7" | 20'5" | 24'0" | 22'-2" | 21'-2" | 20'0" | 25'-2" | 23'4" | 22'-2" | 21'0" |
|  | $16 "$ | 25'6" | 23'6" | 22'-5" | 21'-2" | 26'9" | 24'-8" | 23'6" | 22'-2" | 26-1" | 24'-2" | 23-0" | 21'-9" | 27'-5" | 25'-5" | 24'3" | 22'-11" |
| PWI 52S, LPI 52Plus | 11-7/8" | 21'7" | 20'0" | 19'0" | 18'0" | 22'-8" | 20-11" | 19'-11" | 18'-10" | 22'-1" | 20'6" | 19'6" | 18'5" | 23'-2" | 21'6" | 20'5" | 19'4" |
|  | $14{ }^{\prime \prime}$ | 24'0" | 22'-2" | 21-1" | 19'-11" | 25'-2" | 23-3" | 22'-1" | 20'-11" | 24'-6" | 22'-9" | 21'-8" | 20'6" | 25'9" | 23-10" | 22'-9" | 21'6" |
|  | 16 | 26'1" | 24'1" | 22'-11" | 21'-8" | 27'-5" | 25'4" | 24'-1" | 22'-9" | 26'8" | 24'-9" | 23'7" | 22'-3" | 28'-1" | 26'0" | 24-9" | 23'-5" |
| PWI 56L, LPI 56 | 11-7/8" | 22'-1" | $20^{\prime}-4^{\prime \prime}$ | 19'-4" | 18'-4" | 23'-2" | 21'4" | 20'4" | 19'-2" | 22'-6" | 20'-10" | 19'-10" | 18'9" | 23'-8" | 21'-11" | 20'10" | 19'-8" |
|  | 14" | 24'-5" | 22'7" | 21'-5" | 20'3" | 25'8' | 23'-8" | 22'6" | 21'-3" | 25'0" | 23'1' | 22'-0" | 20'9" | 26-3" | 24'-3" | 23'1" | 21'-10" |
|  | $16 "$ | $26^{\prime}-7{ }^{\prime \prime}$ | $24^{\prime}$-6" | 23'-3" | 22'0" | 27-11" | 25'-9" | $24^{\prime}-6{ }^{\prime \prime}$ | 23'1" | 27-2" | 25'2" | 23'11" | $22^{\prime}-7{ }^{\prime \prime}$ | 28'6" | 26'-5" | 25'-2" | 23'-9" |

## Design Assumptions:

1. The spans listed are the clear distance between supports. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform floor loads only, for standard load duration
3. These tables reflect the additional stiffness for vibration provided by a $3 / 4$ OSB rated sheathing, or equal, attached as indicated (Nailed Only or Clued \& Nailed) to the top flange.
4. Live load deflection is limited to $\mathrm{L} / 360$ "bare joist."
5. Total load deflection is limited to L/240.
6. The spans are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing resistance of an SPF wall plate.

## Additional Notes:

1. These spans have been designed to meet the Limit States Design and vibration requirements of the National Building Code of Canada.
2. Web stiffeners are not required for any of the spans in these tables.
3. Web fillers are required for I-Joists seated in hangers that do not laterally support the top flange.
4. For conditions not shown, use the Uniform Floor Load (PLF) tables, use the Exacte by PWI software or contact your PWT"' distributor for assistance.

# Uniform Floor Load (PLF) Tables: 9½" \& 117/8" 

| Span | 9-1/2" PWI 18S, LPI 18 |  |  | 9-1/2" PWI 20S, LPI 20Plus |  |  | 9-1/2" PWI 32S, LPI 32Plus |  |  | 9-1/2" PWI 42S, LPI 42Plus |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | Factored Total Load | Deflection |  | $\begin{gathered} \text { Factored } \\ \text { Total } \\ \text { Load } \end{gathered}$ | Deflection |  | $\begin{aligned} & \text { Factored } \\ & \text { Total } \\ & \text { Load } \end{aligned}$ | Deflection |  | Factored Total Load |
|  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  |
| 8' | 231 |  | 303 | 284 |  | 337 | 323 |  | 337 |  |  | 424 |
| 9' | 171 |  | 270 | 212 |  | 301 | 243 |  | 301 | 331 |  | 377 |
| 10' | 129 |  | 244 | 161 |  | 271 | 186 |  | 271 | 256 |  | 339 |
| 11' | 100 | 200 | 222 | 125 |  | 247 | 145 |  | 247 | 202 |  | 308 |
| 12' | 78 | 157 | 201 | 99 | 199 | 227 | 116 |  | 227 | 161 |  | 282 |
| 13' | 63 | 126 | 172 | 80 | 160 | 209 | 93 | 187 | 209 | 131 |  | 260 |
| 14' | 51 | 102 | 149 | 65 | 130 | 185 | 76 | 153 | 195 | 107 | 215 | 242 |
| 15' | 42 | 84 | 130 | 53 | 107 | 161 | 63 | 126 | 182 | 89 | 179 | 225 |
| $16^{\prime}$ | 35 | 70 | 114 | 45 | 90 | 142 | 52 | 105 | 169 | 75 | 150 | 211 |
| $17^{\prime}$ | 29 | 59 | 101 | 37 | 75 | 126 | 44 | 89 | 150 | 63 | 127 | 199 |
| 18' | 25 | 50 | 90 | 32 | 64 | 112 | 38 | 76 | 134 | 54 | 108 | 188 |
| 19' | 21 | 43 | 81 | 27 | 55 | 101 | 32 | 65 | 120 | 46 | 93 | 178 |
| 20' | 18 | 37 | 73 | 23 | 47 | 91 | 28 | 56 | 109 | 40 | 80 | 169 |
| $21^{\prime}$ | 16 | 32 | 66 | 20 | 41 | 83 | 24 | 49 | 99 | 35 | 70 | 159 |
| 22' | - | - | - | 18 | 36 | 75 | 21 | 42 | 90 | 30 | 61 | 145 |
| 23' | - | - | - | 15 | 31 | 69 | 18 | 37 | 82 | 27 | 54 | 132 |
| 24' | - | - | - | - | - | - | 16 | 33 | 76 | 23 | 47 | 122 |
| 25' | - | - | - | - | - | - | - | - | - | 21 | 42 | 112 |
| 26' | - | - | - | - | - | - | - | - | - | 19 | 38 | 104 |
| 27' | - | - | - | - | - | - | - | - | - | 17 | 34 | 96 |
| 28' | - | - | - | - | - | - | - | - | - | 15 | 30 | 89 |

Table Usage:

1. Select the span required.
2. Compare the factored design total load to the Factored Total Load column.
3. Compare the specified design total load to the Total L/240 column.
4. Compare the specified design live load to the Live L/480 column. For a live load deflection limit of $L / 360$, refer to Additional Note 4 below.
5. Select a product that satisfies all three conditions.

## Example:

Select an 1 -Joist for a $17^{\prime}$-6" clear span supporting specified loads of 40 psf Live Load and 20 psf Dead Load, spaced 16" oc, at an L/480 deflection limit.

1. Factored Total Load $=(1.50 \times 40+1.25 \times 20)^{*}$
( $16 / 12$ ) $=114 \mathrm{plf}$
Unfactored Total Load $=(40+20)^{*}(16 / 12)=80$ plf Unfactored Live Load $=40 *(16 / 12)=54$ plf
2. Select the row corresponding to an 18 'span.
3. Select the first joist to exceed all three resistance criteria: The 9-1/2" PWI $42 S$ supports 185 plf Factored Total Load, 108 plf Total L/240 Deflection and 54 plf Live L/480 Deflection resistance.

| Span | $\begin{gathered} \text { 11-7/8" PWI 18S, } \\ \text { LPI } 18 \end{gathered}$ |  |  | $\begin{gathered} \text { 11-7/8" PWI 20S, } \\ \text { LPI 20Plus } \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \text { 11-7/8" PW\| 32S, } \\ \text { LPI 32Plus } \\ \hline \end{gathered}$ |  |  | $\begin{gathered} 11-7 / 8^{1 " ~ P W I I ~ 36 L, ~} \\ \text { LPI } 36 \end{gathered}$ |  |  | $\begin{gathered} \text { 11-7/8" PWV 42S, } \\ \text { LPP 42Plus } \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \text { 11-7/8" PWV 52S, } \\ \text { LPI 52Plus } \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \text { 11-7/8" PWII 56L, } \\ \text { LPI } 56 \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | $\begin{gathered} \text { Factored } \\ \text { Total } \\ \text { Load } \end{gathered}$ | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load |
|  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Total } \\ \text { L/240 } \\ \hline \end{array}$ |  | $\begin{array}{\|c} \hline \text { Live } \\ \text { L/480 } \\ \hline \end{array}$ | $\begin{array}{\|c} \hline \text { Total } \\ \text { L/240 } \\ \hline \end{array}$ |  | $\begin{array}{\|l} \hline \text { Live } \\ \text { L/480 } \\ \hline \end{array}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{array}{\|l\|l\|} \hline \text { Live } \\ \text { L/480 } \end{array}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{array}{\|c} \hline \text { Live } \\ \text { L/480 } \end{array}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  |
| $8^{\prime}$ |  |  | 322 |  |  | 358 |  |  | 358 |  |  | 384 |  |  | 465 |  |  | 526 |  |  | 449 |
| $9 '$ | 278 |  | 287 |  |  | 319 |  |  | 319 |  |  | 342 |  |  | 414 |  |  | 469 |  |  | 401 |
| 10' | 212 |  | 259 | 258 |  | 288 |  |  | 288 |  |  | 308 |  |  | 374 |  |  | 423 |  |  | 362 |
| $11^{\prime}$ | 166 |  | 235 | 203 |  | 262 | 231 |  | 262 | 260 |  | 281 | 319 |  | 340 | 361 |  | 385 |  |  | 330 |
| 12' | 131 |  | 216 | 162 |  | 241 | 185 |  | 241 | 209 |  | 258 | 258 |  | 312 | 290 |  | 353 |  |  | 303 |
| 13' | 106 |  | 200 | 131 |  | 222 | 150 |  | 222 | 170 |  | 238 | 210 |  | 289 | 236 |  | 327 | 249 |  | 280 |
| 14' | 86 | 173 | 176 | 107 |  | 207 | 124 |  | 207 | 140 |  | 221 | 174 |  | 268 | 195 |  | 304 | 207 |  | 260 |
| 15' | 71 | 143 | 153 | 89 | 178 | 193 | 103 |  | 193 | 116 |  | 207 | 145 |  | 251 | 162 |  | 284 | 173 |  | 243 |
| 16' | 59 | 119 | 135 | 74 | 149 | 181 | 86 | 173 | 181 | 98 |  | 194 | 122 |  | 235 | 136 |  | 266 | 146 |  | 228 |
| 17' | 50 | 101 | 120 | 63 | 126 | 168 | 73 | 146 | 171 | 83 | 166 | 183 | 104 | 208 | 222 | 116 | 232 | 251 | 124 |  | 215 |
| 18' | 42 | 85 | 107 | 54 | 108 | 150 | 62 | 125 | 161 | 71 | 142 | 173 | 89 | 178 | 209 | 99 | 198 | 237 | 107 |  | 203 |
| 19' | 36 | 73 | 96 | 46 | 92 | 135 | 53 | 107 | 153 | 61 | 122 | 164 | 76 | 153 | 198 | 85 | 170 | 224 | 92 | 184 | 193 |
| $20^{\prime}$ | 31 | 63 | 87 | 40 | 80 | 122 | 46 | 93 | 141 | 53 | 106 | 155 | 66 | 133 | 189 | 74 | 148 | 213 | 80 | 160 | 183 |
| $21^{\prime}$ | 27 | 55 | 79 | 34 | 69 | 111 | 40 | 81 | 128 | 46 | 92 | 148 | 58 | 116 | 180 | 64 | 129 | 203 | 70 | 140 | 175 |
| 22' | 24 | 48 | 72 | 30 | 61 | 101 | 35 | 71 | 116 | 40 | 81 | 141 | 51 | 102 | 172 | 56 | 113 | 194 | 61 | 123 | 167 |
| 23' | 21 | 42 | 66 | 26 | 53 | 92 | 31 | 62 | 107 | 35 | 71 | 135 | 45 | 90 | 164 | 49 | 99 | 186 | 54 | 109 | 160 |
| $24^{\prime}$ | 18 | 37 | 60 | 23 | 47 | 85 | 27 | 55 | 98 | 31 | 63 | 130 | 40 | 80 | 157 | 44 | 88 | 178 | 48 | 96 | 153 |
| $25^{\prime}$ | 16 | 33 | 56 | 21 | 42 | 78 | 24 | 49 | 90 | 28 | 56 | 125 | 35 | 71 | 145 | 39 | 78 | 171 | 43 | 86 | 147 |
| $26^{\prime}$ |  |  |  | 18 | 37 | 72 | 22 | 44 | 83 | 25 | 50 | 120 | 31 | 63 | 134 | 35 | 70 | 164 | 38 | 77 | 141 |
| 27' |  |  |  | 16 | 33 | 67 | 19 | 39 | 77 | 22 | 45 | 115 | 28 | 57 | 125 | 31 | 63 | 152 | 34 | 69 | 136 |
| $28^{\prime}$ | - | - | - | 15 | 30 | 62 | 17 | 35 | 72 | 20 | 40 | 107 | 25 | 51 | 116 | 28 | 56 | 141 | 31 | 62 | 131 |

## Design Assumptions:

1. Span is the clear distance between supports and is valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The values in the tables are for uniform loads only.
3. Factored Total Load resistance is for standard ( $100 \%$ ) load duration.
4. These tables do not reflect any additional stiffness provided by the floor sheathing.
5. Live L/480 Deflection resistance is limited to L/480. Vibration has not been considered.
6. Total L/240 Deflection resistance is limited to $\mathrm{L} / 240$. Long term deflection (creep) has not been considered.
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24."
8. These tables are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least 3-1/2," and are limited to the bearing capacity for an SPF wall plate.

## Additional Notes:

1. These tables have been designed to meet the Limit States Design requirements of the National Building Code of Canada.
2. The tabulated resistances represent the capacity of the member in pounds per lineal foot (plf) of length.
3. The designer shall check the Factored Total Load, the Total L/240 Deflection and the Live L/480 Deflection resistance columns.
4. To design for an $\mathrm{L} / 360$ live load deflection, multiply the Live $\mathrm{L} / 480$ Deflection values by 1.33 or refer to the Uniform Roof Load (PLF) Tables on page 11.
5. Where the Deflection resistance is blank, the Factored Total Load resistance governs the design.
6. To design a double l-Joist, the values in these tables can be doubled, or the design loads on the I-Joist may be halved to verify the capacity of each ply. The capacity is additive.
7. Web stiffeners are not required for these spans and loads.
8. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require nailing into the web.
9. Do not use a product where designated """ without further analysis by a design professional.

## PSF TO PLF CONVERSION

| $0 C$ Spacing | Load |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20 psf | 25 psf | 30 psf | 35 psf | 40 psf | 45 psf | 50 psf | 55 psf | 60 psf | 65 psf |
| 12" | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 |
| 16 " | 27 | 34 | 40 | 47 | 54 | 60 | 67 | 74 | 80 | 87 |
| 19.2" | 32 | 40 | 48 | 56 | 64 | 72 | 80 | 88 | 96 | 104 |
| 24 " | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 | 130 |

To Convert from Specified to Factored Total PLF:
Factored Total plf $=1.50 \times$ Specified Live plf $+1.25 \times$ Specified Dead plf

## Uniform Floor Load (PLF) Tables: 14" \& 16" <br> Table Usage: <br> Example: Select an I-Joist for a 20'-6" clear span supporting specified loads of 40 psf Live Load and 20 psf Dead

1. Select the span required.
2. Compare the factored design total load to the Factored Total Load column.
3. Compare the specified design total load to the Total L/240 column.
4. Compare the specified design live load to the Live L/480 column. For a live load deflection limit of L/360, refer to Additional Note 4 below.
5. Select a product that satisfies all three conditions.

Load, spaced 16" oc, at an L/480 deflection limit.

1. Factored Total Load $=(1.50 \times 40+1.25 \times 20) *(16 / 12)=114$ plf

Unfactored Total Load $=(40+20)^{*}(16 / 12)=80$ plf
Unfactored Live Load $=40^{*}(16 / 12)=54$ plf
2. Select the row corresponding to an 21' span.
3. Select the first joist to exceed all three resistance criteria:

The 14" PWI $32 S$ supports 145 plf Factored Total Load, 116 plf Total L/240 Deflection and 58 plf Live
L/480 Deflection resistance.

| Span | 14" PWI 20S, LPI 20Plus |  |  | 14" PWI 32S, LPI 32Plus |  |  | 14" PWII 36L, LPI 36 |  |  | 14" PWI 42S, LPI 42Plus |  |  | 14" PWI 52S, LPI 52Plus |  |  | 14" PWII 56L, LPI 56 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load |
|  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | Total L/240 |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  |
| $14^{\prime}$ | 154 |  | 218 | 174 |  | 218 | 195 |  | 221 | 244 |  | 279 | 273 |  | 305 |  |  | 261 |
| $15^{\prime}$ | 129 |  | 203 | 145 |  | 203 | 163 |  | 207 | 204 |  | 260 | 228 |  | 285 | 240 |  | 244 |
| $16^{\prime}$ | 108 |  | 191 | 122 |  | 191 | 138 |  | 194 | 173 |  | 244 | 193 |  | 267 | 203 |  | 229 |
| $17^{\prime}$ | 91 |  | 180 | 104 |  | 180 | 117 |  | 183 | 147 |  | 230 | 164 |  | 251 | 174 |  | 215 |
| 18' | 78 | 157 | 170 | 89 |  | 170 | 100 |  | 173 | 126 |  | 217 | 140 |  | 238 | 150 |  | 204 |
| 19' | 67 | 135 | 158 | 77 | 154 | 161 | 86 |  | 164 | 109 |  | 206 | 121 |  | 225 | 129 |  | 193 |
| 20' | 58 | 117 | 143 | 66 | 133 | 153 | 75 | 150 | 155 | 95 | 190 | 196 | 105 | 211 | 214 | 113 |  | 184 |
| 21' | 51 | 102 | 130 | 58 | 116 | 146 | 65 | 131 | 148 | 83 | 167 | 186 | 92 | 184 | 204 | 99 |  | 175 |
| 22' | 44 | 89 | 118 | 51 | 102 | 139 | 57 | 115 | 141 | 73 | 146 | 178 | 81 | 162 | 195 | 87 |  | 167 |
| 23' | 39 | 79 | 108 | 45 | 90 | 128 | 51 | 102 | 135 | 64 | 129 | 170 | 71 | 143 | 186 | 77 | 154 | 160 |
| 24' | 35 | 70 | 99 | 40 | 80 | 118 | 45 | 90 | 130 | 57 | 115 | 163 | 63 | 126 | 179 | 68 | 137 | 153 |
| 25' | 31 | 62 | 92 | 35 | 71 | 109 | 40 | 80 | 125 | 51 | 102 | 157 | 56 | 113 | 172 | 61 | 122 | 147 |
| 26' | 27 | 55 | 85 | 31 | 63 | 101 | 36 | 72 | 120 | 46 | 92 | 151 | 50 | 101 | 165 | 54 | 109 | 142 |
| 27' | 24 | 49 | 79 | 28 | 57 | 93 | 32 | 64 | 115 | 41 | 82 | 145 | 45 | 90 | 159 | 49 | 98 | 136 |
| $28^{\prime}$ | 22 | 45 | 73 | 25 | 51 | 87 | 29 | 58 | 111 | 37 | 74 | 140 | 40 | 81 | 153 | 44 | 89 | 131 |
| 29' | 20 | 40 | 68 | 23 | 46 | 81 | 26 | 52 | 107 | 33 | 67 | 130 | 37 | 74 | 148 | 40 | 80 | 127 |
| 30' | 18 | 36 | 64 | 21 | 42 | 76 | 23 | 47 | 104 | 30 | 61 | 122 | 33 | 67 | 143 | 36 | 73 | 123 |
| 31' | 16 | 33 | 60 | 19 | 38 | 71 | 21 | 43 | 101 | 27 | 55 | 114 | 30 | 61 | 138 | 33 | 66 | 119 |
| 32' | 15 | 30 | 56 | 17 | 35 | 66 | 19 | 39 | 97 | 25 | 50 | 107 | 27 | 55 | 130 | 30 | 60 | 115 |
| 33' | - | - | - | 16 | 32 | 62 | 18 | 36 | 93 | 23 | 46 | 101 | 25 | 51 | 123 | 27 | 55 | 112 |
| 34' | - | - | - | - | - | - | 16 | 33 | 88 | 21 | 42 | 95 | 23 | 46 | 115 | 25 | 51 | 108 |


| Span | 16" PWI 20S, LPI 20Plus |  |  | 16" PWI 32S, LPI 32Plus |  |  | 16" PWI 36L, LPI 36 |  |  | 16" PWI 42S, LPI 42Plus |  |  | 16" PWI 52S, LPI 52Plus |  |  | 16" PWII 56L, LPI 56 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load |
|  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & 1 / 240 \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{gathered} \text { Total } \\ \text { L/240 } \\ \hline \end{gathered}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/480 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  |
| 14' | 205 |  | 220 |  |  | 220 |  |  | 221 |  |  | 288 |  |  | 306 |  |  | 261 |
| 15' | 171 |  | 205 | 191 |  | 205 |  |  | 207 | 268 |  | 269 |  |  | 286 |  |  | 244 |
| $16^{\prime}$ | 145 |  | 193 | 161 |  | 193 | 180 |  | 194 | 227 |  | 252 | 253 |  | 268 |  |  | 229 |
| $17^{\prime}$ | 123 |  | 181 | 137 |  | 181 | 153 |  | 183 | 195 |  | 238 | 216 |  | 253 |  |  | 216 |
| $18 '$ | 105 |  | 171 | 118 |  | 171 | 132 |  | 173 | 167 |  | 224 | 185 |  | 239 | 195 |  | 204 |
| 19' | 91 |  | 163 | 102 |  | 163 | 114 |  | 164 | 145 |  | 213 | 160 |  | 226 | 169 |  | 193 |
| 20' | 79 |  | 154 | 88 |  | 154 | 99 |  | 155 | 126 |  | 202 | 139 |  | 215 | 148 |  | 184 |
| 21' | 69 | 138 | 147 | 77 |  | 147 | 86 |  | 148 | 111 |  | 193 | 122 |  | 205 | 130 |  | 175 |
| 22' | 60 | 121 | 136 | 68 | 136 | 141 | 76 |  | 141 | 98 |  | 184 | 107 |  | 196 | 114 |  | 167 |
| $23 '$ | 53 | 107 | 124 | 60 | 120 | 135 | 67 |  | 135 | 86 | 173 | 176 | 95 |  | 187 | 101 |  | 160 |
| 24' | 47 | 95 | 114 | 53 | 107 | 129 | 60 | 120 | 130 | 77 | 154 | 169 | 84 | 169 | 179 | 90 |  | 153 |
| 25' | 42 | 84 | 105 | 47 | 95 | 124 | 53 | 107 | 125 | 68 | 137 | 162 | 75 | 151 | 172 | 80 |  | 147 |
| 26 | 37 | 75 | 97 | 42 | 85 | 117 | 47 | 95 | 120 | 61 | 123 | 156 | 67 | 135 | 166 | 72 |  | 142 |
| 27 | 33 | 67 | 90 | 38 | 76 | 108 | 43 | 86 | 115 | 55 | 111 | 150 | 60 | 121 | 160 | 65 | 130 | 137 |
| 28 | 30 | 61 | 84 | 34 | 69 | 101 | 38 | 77 | 111 | 50 | 100 | 145 | 54 | 109 | 154 | 59 | 118 | 132 |
| 29' | 27 | 55 | 78 | 31 | 62 | 94 | 35 | 70 | 107 | 45 | 90 | 140 | 49 | 99 | 149 | 53 | 107 | 127 |
| 30' | 25 | 50 | 73 | 28 | 56 | 88 | 31 | 63 | 104 | 41 | 82 | 135 | 45 | 90 | 144 | 48 | 97 | 123 |
| 31' | 22 | 45 | 68 | 25 | 51 | 82 | 29 | 58 | 101 | 37 | 75 | 131 | 40 | 81 | 139 | 44 | 88 | 119 |
| 32' | 20 | 41 | 64 | 23 | 47 | 77 | 26 | 52 | 97 | 34 | 68 | 124 | 37 | 74 | 135 | 40 | 80 | 115 |
| 33' | 19 | 38 | 60 | 21 | 43 | 73 | 24 | 48 | 94 | 31 | 62 | 117 | 34 | 68 | 131 | 37 | 74 | 112 |
| 34' | 17 | 34 | 57 | 19 | 39 | 68 | 22 | 44 | 92 | 28 | 57 | 110 | 31 | 62 | 127 | 34 | 68 | 109 |

## Design Assumptions:

1. Span is the clear distance between supports and is valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The values in the tables are for uniform loads only.
3. Factored Total Load resistance is for standard ( $100 \%$ ) load duration.
4. These tables do not reflect any additional stiffness provided by the floor sheathing.
5. Live $\mathrm{L} / 480$ Deflection resistance is limited to $\mathrm{L} / 480$. Vibration has not been considered
6. Total L/240 Deflection resistance is limited to L/240. Long term deflection (creep) has not been considered
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24."
8. These tables are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing capacity for an SPF wall plate.
PSF TO PLF CONVERSION

| OC Spacing | Load |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20 psf | 25 psf | 30 psf | 35 psf | 40 psf | 45 psf | 50 psf | 55 psf | 60 psf | 65 psf |
| 12 " | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 |
| $16 "$ | 27 | 34 | 40 | 47 | 54 | 60 | 67 | 74 | 80 | 87 |
| 19.2" | 32 | 40 | 48 | 56 | 64 | 72 | 80 | 88 | 96 | 104 |
| 24 " | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 | 130 |

## ddditional Notes:

1. These tables have been designed to meet the Limit States Design requirements of the National Building Code of Canada.
2. The tabulated resistances represent the capacity of the member in pounds per lineal foot (plf) of length.
3. The designer shall check the Factored Total Load, the Total L/240 Deflection and the Live L/480 Deflection resistance columns.
4. To design for an L/360 live load deflection, multiply the Live L/480 Deflection values by 1.33 or refer to the Uniform Roof Load (PLF) Tables on page 12
5. Where the Deflection resistance is blank, the Factored Total Load resistance governs the design.
6. To design a double l-Joist, the values in these tables can be doubled, or the design loads on the l-Joist may be halved to verify the capacity of each ply. The capacity is additive.
7. Web stiffeners are not required for these spans and loads.
8. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require nailing into the web.
9. Do not use a product where designated "" "without further analysis by a design professional.

## Uniform Roof Load (PLF) Tables: 9½" \& 117/8"

| Span | 9-1/2" PWI 18S, LPI 18 |  |  | 9-1/2" PWI 20S, LPI 20Plus |  |  | 9-1/2" PWI 32S, LPI 32Plus |  |  | 9-1/2" PWI 42S, LPI 42Plus |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load |
|  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \mathrm{L} / 360 \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \\ & \hline \end{aligned}$ |  |
| 8' |  |  | 303 |  |  | 337 |  |  | 337 |  |  | 424 |
| 9' | 228 |  | 270 | 282 |  | 301 |  |  | 301 |  |  | 377 |
| $10^{\prime}$ | 172 |  | 244 | 215 |  | 271 | 248 |  | 271 |  |  | 339 |
| 11' | 133 |  | 222 | 167 |  | 247 | 194 |  | 247 | 269 |  | 308 |
| 12' | 105 |  | 201 | 132 |  | 227 | 154 |  | 227 | 215 |  | 282 |
| $13 '$ | 84 | 168 | 172 | 106 |  | 209 | 124 |  | 209 | 175 |  | 260 |
| $14^{\prime}$ | 68 | 137 | 149 | 87 | 174 | 185 | 102 |  | 195 | 143 |  | 242 |
| $15^{\prime}$ | 56 | 112 | 130 | 71 | 143 | 161 | 84 | 168 | 182 | 119 |  | 225 |
| $16^{\prime}$ | 46 | 93 | 114 | 60 | 120 | 142 | 70 | 141 | 169 | 100 | 200 | 211 |
| $17{ }^{\prime}$ | 39 | 78 | 101 | 50 | 101 | 126 | 59 | 119 | 150 | 84 | 169 | 199 |
| 18' | 33 | 67 | 90 | 43 | 86 | 112 | 50 | 101 | 134 | 72 | 144 | 188 |
| 19' | 28 | 57 | 81 | 36 | 73 | 101 | 43 | 87 | 120 | 62 | 124 | 178 |
| $20^{\prime}$ | 24 | 49 | 73 | 31 | 63 | 91 | 37 | 75 | 109 | 53 | 107 | 169 |
| 21' | 21 | 42 | 66 | 27 | 55 | 83 | 32 | 65 | 99 | 46 | 93 | 159 |
| $22^{\prime}$ | 18 | 37 | 60 | 24 | 48 | 75 | 28 | 57 | 90 | 41 | 82 | 145 |
| $23^{\prime}$ | 16 | 32 | 55 | 21 | 42 | 69 | 25 | 50 | 82 | 36 | 72 | 132 |
| $24^{\prime}$ | - | - | - | 18 | 37 | 63 | 22 | 44 | 76 | 31 | 63 | 122 |
| $25^{\prime}$ | - | - | - | 16 | 33 | 58 | 19 | 39 | 70 | 28 | 56 | 112 |
| $26^{\prime}$ | - | - | - | - | - | - | 17 | 35 | 64 | 25 | 50 | 104 |
| 27 | - | - | - | - | - | - | 15 | 31 | 60 | 22 | 45 | 96 |
| 28 ' | - | - | - | - | - | - | - | - | - | 20 | 40 | 89 |

Table Usage:

1. Select the span required. For roofs with a slope of 2:12 or greater, the horizontal span shall be multiplied by the appropriate roof pitch adjustment factor from the table at the bottom of this page.
2. Compare the factored design total load to the Factored Total Load column.
3. Compare the specified design total load to the Total L/180 column.
4. Compare the specified design live load to the Live L/360 column. For a live load deflection limit of L/480 or L/240, refer to Additional Note 5 below.
5. Select a product that satisfies all three conditions.

Example: Select an I-Joist for a 12'-8" horizontal clear span supporting 45 psf Snow (Live) Load and 15 psf Dead Load, spaced 24" oc, with a roof slope of $6: 12$, at an L/360 deflection limit.

1. Factored Total Load $=(1.50 \times 45+1.25 \times 15)^{*}(24 / 12)=173$ plf Unfactored Total Load $=(45+15)^{*}(24 / 12)=120$ plf Unfactored Live Load $=45^{*}(24 / 12)=90$ plf
2. Sloped Span $=(12+8 / 12) * 1.118=14.16^{\prime}$
3. Select the row corresponding to a 15 ' span.
4. Select the first joist to exceed all three resistance criteria:

The 9-1/2" PWI 425 supports 222 plf Factored Total Load and 118 plf Live L/360 Deflection. Total L/180 Deflection does not control.

| Span | $\begin{gathered} \text { 11-7/8" PWI 18S, } \\ \text { LPI } 18 \end{gathered}$ |  |  | 11-7/8" PWI 20S, LPI 2OPlus |  |  | $\begin{gathered} \text { 11-7/8" PWI 32S, } \\ \text { LPI 32Plus } \end{gathered}$ |  |  | $\begin{gathered} \text { 11-7/8" PWII 36L, } \\ \text { LPI } 36 \\ \hline \end{gathered}$ |  |  | 11-7/8" PWI 42S,LPI 42Plus |  |  | $\begin{aligned} & \text { 11-7/8" PWII 52S, } \\ & \text { LPI 52Plus } \\ & \hline \end{aligned}$ |  |  | $\begin{gathered} \text { 11-7/8" PWI 56L, } \\ \text { LPI } 56 \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load |
|  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{gathered} \text { Live } \\ \text { L/360 } \end{gathered}$ | Total L/180 |  |
| 8' |  |  | 322 |  |  | 358 |  |  | 358 |  |  | 384 |  |  | 465 |  |  | 526 |  |  | 449 |
| 9' |  |  | 287 |  |  | 319 |  |  | 319 |  |  | 342 |  |  | 414 |  |  | 469 |  |  | 401 |
| 10' |  |  | 259 |  |  | 288 |  |  | 288 |  |  | 308 |  |  | 374 |  |  | 423 |  |  | 362 |
| 11' | 221 |  | 235 |  |  | 262 |  |  | 262 |  |  | 281 |  |  | 340 |  |  | 385 |  |  | 330 |
| $12^{\prime}$ | 175 |  | 216 | 216 |  | 241 |  |  | 241 |  |  | 258 |  |  | 312 |  |  | 353 |  |  | 303 |
| $13 '$ | 141 |  | 200 | 175 |  | 222 | 201 |  | 222 | 227 |  | 238 | 281 |  | 289 | 315 |  | 327 |  |  | 280 |
| $14^{\prime}$ | 115 |  | 176 | 143 |  | 207 | 165 |  | 207 | 187 |  | 221 | 232 |  | 268 | 260 |  | 304 |  |  | 260 |
| $15 '$ | 95 |  | 153 | 119 |  | 193 | 137 |  | 193 | 155 |  | 207 | 194 |  | 251 | 216 |  | 284 | 231 |  | 243 |
| 16 ' | 79 |  | 135 | 99 |  | 181 | 115 |  | 181 | 131 |  | 194 | 163 |  | 235 | 182 |  | 266 | 195 |  | 228 |
| $17^{\prime}$ | 67 |  | 120 | 84 |  | 168 | 97 |  | 171 | 111 |  | 183 | 138 |  | 222 | 154 |  | 251 | 166 |  | 215 |
| $18^{\prime}$ | 57 |  | 107 | 72 | 144 | 150 | 83 |  | 161 | 94 |  | 173 | 118 |  | 209 | 132 |  | 237 | 142 |  | 203 |
| 19' | 49 |  | 96 | 61 | 123 | 135 | 71 | 143 | 153 | 81 | 163 | 164 | 102 |  | 198 | 113 |  | 224 | 123 |  | 193 |
| $20^{\prime}$ | 42 | 84 | 87 | 53 | 107 | 122 | 62 | 124 | 141 | 70 | 141 | 155 | 89 | 178 | 189 | 98 | 197 | 213 | 107 |  | 183 |
| 21' | 36 | 73 | 79 | 46 | 93 | 111 | 54 | 108 | 128 | 61 | 123 | 148 | 77 | 155 | 180 | 86 | 172 | 203 | 93 |  | 175 |
| 22' | 32 | 64 | 72 | 40 | 81 | 101 | 47 | 95 | 116 | 54 | 108 | 141 | 68 | 136 | 172 | 75 | 151 | 194 | 82 | 164 | 167 |
| 23' | 28 | 56 | 66 | 35 | 71 | 92 | 41 | 83 | 107 | 47 | 95 | 135 | 60 | 120 | 164 | 66 | 133 | 186 | 72 | 145 | 160 |
| $24^{\prime}$ | 25 | 50 | 60 | 31 | 63 | 85 | 37 | 74 | 98 | 42 | 84 | 130 | 53 | 106 | 157 | 59 | 118 | 178 | 64 | 128 | 153 |
| $25^{\prime}$ | 22 | 44 | 56 | 28 | 56 | 78 | 33 | 66 | 90 | 37 | 75 | 125 | 47 | 95 | 145 | 52 | 105 | 171 | 57 | 114 | 147 |
| $26^{\prime}$ | 19 | 39 | 51 | 25 | 50 | 72 | 29 | 59 | 83 | 33 | 67 | 120 | 42 | 85 | 134 | 46 | 93 | 164 | 51 | 102 | 141 |
| 27 | 17 | 35 | 48 | 22 | 45 | 67 | 26 | 52 | 77 | 30 | 60 | 115 | 38 | 76 | 125 | 42 | 84 | 152 | 46 | 92 | 136 |
| 28' | 16 | 32 | 44 | 20 | 40 | 62 | 23 | 47 | 72 | 27 | 54 | 107 | 34 | 68 | 116 | 37 | 75 | 141 | 41 | 83 | 131 |

Design Assumptions:

1. Span is the clear distance between supports and is valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The values in the tables are for uniform loads only.
3. Factored Total Load resistance is for standard ( $100 \%$ ) load duration.
4. These tables do not reflect any additional stiffness provided by the sheathing.
5. Live $\mathrm{L} / 360$ Deflection resistance is limited to $\mathrm{L} / 360$. Vibration has not been considered.
6. Total L/180 Deflection resistance is limited to L/180. Long term deflection (creep) has not been considered.
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24 ."
8. These tables are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing capacity for an SPF wall plate.

## Additional Notes:

1. These tables have been designed to meet the Limit States Design requirements of the National Building Code of Canada.
2. The tabulated resistances represent the capacity of the member in pounds per lineal foot (plf) of length.
3. For roofs with a slope of $2: 12$ or greater, the horizontal span shall be multiplied by the appropriate pitch adjustment factor from the table at the bottom of this page. Roof joists shall have a minimum pitch of $1 / 4^{\prime \prime}$ per foot (1/4:12) for positive drainage.
4. The designer shall check the Factored Total Load, the Total L/180 Deflection and the Live L/360 Deflection resistance columns.
5. To design for an $\mathrm{L} / 240$ live load deflection, multiply the Live $\mathrm{L} / 360$ Deflection values by 1.5 . To design for a L/480 live load deflection, multiply the Live L/360 Deflection values by 0.75 or refer to the Uniform Floor Load (PLF) Tables on page 9.
6. Where the Deflection resistance is blank, the Factored Total Load resistance governs the design.
7. To design a double 1 -Joist, the values in these tables can be doubled, or the design loads on the 1 -Joist may be halved to verify the capacity of each ply. The capacity is additive.
8. Web stiffeners are not required for these spans and loads.
9. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require naling into the web.
10. Do not use a product where designated """ without further analysis by a design professional.

| Roof <br> Pitch | $2: 12$ | $3: 12$ | $4: 12$ | $5: 12$ | $6: 12$ | $7: 12$ | $8: 12$ | $9: 12$ | $10: 12$ | $11: 12$ | $12: 12$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Factor | 1.014 | 1.031 | 1.054 | 1.083 | 1.118 | 1.158 | 1.202 | 1.250 | 1.302 | 1.357 | 1.414 |

# Uniform Roof Load (PLF) Tables: 14" \& 16" 

Table Usage:
Select the span required. For roofs with a pitch of 2:12 or greater, the horizontal span shall be multiplied by the appropriate roof pitch adjustment factor from the table at the bottom of this page.
2. Compare the factored design total load to the Factored Total Load column.
3. Compare the specified design total load to the Total L/180 column.
4. Compare the specified design live load to the Live L/360 column. For a live load deflection limit of $\mathrm{L} / 480$ or $\mathrm{L} / 240$, refer to Additional Note 5 below.
5. Select a product that satisfies all three conditions.

Example: Select an I-Joist for a 17'-8" horizontal clear span supporting 45 psf Snow (Live) Load and 15 psf Dead Load, spaced 24" oc, with a roof pitch of $6: 12$, at an L/360 deflection limit.

1. Factored Total Load $=(1.50 \times 45+1.25 \times 15)^{*}(24 / 12)=173 \mathrm{plf}$

Unfactored Total Load $=(45+15)^{*}(24 / 12)=120$ plf
Unfactored Live Load $=45^{*}(24 / 12)=90$ plf
2. Sloped Span $=(17+8 / 12)^{*} 1.118=19.75^{\prime}$
3. Select the row corresponding to a 20 ' span.
4. Select the first joist to exceed all three resistance criteria:

The 14" PWI 42 s supports 195 plf Factored Total Load and 126 plf Live L/360 Deflection. Total L/180 Deflection does not control.

| Span | 14" PWI 20S, LPI 20Plus |  |  | 14" PWII 32S, LPI 32Plus |  |  | 14" PWI 36L, LPI 36 |  |  | 14" PWI 42S, LPI 42Plus |  |  | 14" PWI 52S, LPI 52Plus |  |  | 14" PWI 56L, LPI 56 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load |
|  | $\begin{gathered} \text { Live } \\ \text { L/360 } \end{gathered}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | Total L/180 |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | Total L/180 |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | Total L/180 |  | Live L/360 | Total L/180 |  |
| $14^{\prime}$ | 206 |  | 218 |  |  | 218 |  |  | 221 |  |  | 279 |  |  | 305 |  |  | 261 |
| $15^{\prime}$ | 172 |  | 203 | 194 |  | 203 |  |  | 207 |  |  | 260 |  |  | 285 |  |  | 244 |
| $16^{\prime}$ | 144 |  | 191 | 163 |  | 191 | 184 |  | 194 | 231 |  | 244 | 257 |  | 267 |  |  | 229 |
| $17{ }^{\prime}$ | 122 |  | 180 | 139 |  | 180 | 156 |  | 183 | 197 |  | 230 | 218 |  | 251 |  |  | 215 |
| 18' | 104 |  | 170 | 119 |  | 170 | 134 |  | 173 | 169 |  | 217 | 187 |  | 238 | 200 |  | 204 |
| 19' | 90 |  | 158 | 102 |  | 161 | 115 |  | 164 | 146 |  | 206 | 162 |  | 225 | 173 |  | 193 |
| 20' | 78 |  | 143 | 89 |  | 153 | 100 |  | 155 | 127 |  | 196 | 140 |  | 214 | 150 |  | 184 |
| 21' | 68 |  | 130 | 77 |  | 146 | 87 |  | 148 | 111 |  | 186 | 123 |  | 204 | 132 |  | 175 |
| 22' | 59 |  | 118 | 68 | 136 | 139 | 77 |  | 141 | 97 |  | 178 | 108 |  | 195 | 116 |  | 167 |
| 23 ' | 52 | 105 | 108 | 60 | 120 | 128 | 68 |  | 135 | 86 |  | 170 | 95 |  | 186 | 103 |  | 160 |
| $24^{\prime}$ | 46 | 93 | 99 | 53 | 107 | 118 | 60 | 120 | 130 | 76 | 153 | 163 | 84 | 169 | 179 | 91 |  | 153 |
| 25 | 41 | 83 | 92 | 47 | 95 | 109 | 53 | 107 | 125 | 68 | 137 | 157 | 75 | 150 | 172 | 81 |  | 147 |
| $26^{\prime}$ | 37 | 74 | 85 | 42 | 85 | 101 | 48 | 96 | 120 | 61 | 122 | 151 | 67 | 134 | 165 | 73 |  | 142 |
| 27' | 33 | 66 | 79 | 38 | 76 | 93 | 43 | 86 | 115 | 55 | 110 | 145 | 60 | 121 | 159 | 65 | 131 | 136 |
| $28^{\prime}$ | 30 | 60 | 73 | 34 | 68 | 87 | 38 | 77 | 111 | 49 | 99 | 140 | 54 | 109 | 153 | 59 | 118 | 131 |
| 29' | 27 | 54 | 68 | 31 | 62 | 81 | 35 | 70 | 107 | 44 | 89 | 130 | 49 | 98 | 148 | 53 | 107 | 127 |
| $30^{\prime}$ | 24 | 49 | 64 | 28 | 56 | 76 | 31 | 63 | 104 | 40 | 81 | 122 | 44 | 89 | 143 | 48 | 97 | 123 |
| 31' | 22 | 44 | 60 | 25 | 51 | 71 | 29 | 58 | 101 | 37 | 74 | 114 | 40 | 81 | 138 | 44 | 88 | 119 |
| $32^{\prime}$ | 20 | 40 | 56 | 23 | 46 | 66 | 26 | 53 | 97 | 33 | 67 | 107 | 37 | 74 | 130 | 40 | 81 | 115 |
| 33' | 18 | 37 | 53 | 21 | 42 | 62 | 24 | 48 | 93 | 31 | 62 | 101 | 34 | 68 | 123 | 37 | 74 | 112 |
| 34' | 17 | 34 | 50 | 19 | 39 | 59 | 22 | 44 | 88 | 28 | 56 | 95 | 31 | 62 | 115 | 34 | 68 | 108 |


| Span | 16" PWI 20S, LPI 20Plus |  |  | 16" PWI 32S, LPI 32Plus |  |  | 16" PWII 36L, LPI 36 |  |  | 16" PWI 42S, LPI 42Plus |  |  | 16" PWI 52S, LPI 52Plus |  |  | 16" PWI 56L, LPI 56 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load | Deflection |  | Factored Total Load |
|  | $\begin{gathered} \text { Live } \\ \text { L/360 } \end{gathered}$ | $\begin{array}{r} \text { Total } \\ \text { L/180 } \\ \hline \end{array}$ |  | $\begin{gathered} \text { Live } \\ \text { L/360 } \end{gathered}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | Total L/180 |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | Total L/180 |  | $\begin{aligned} & \text { Live } \\ & \text { L/360 } \end{aligned}$ | Total L/180 |  |
| 14' |  |  | 220 |  |  | 220 |  |  | 221 |  |  | 288 |  |  | 306 |  |  | 261 |
| 15' |  |  | 205 |  |  | 205 |  |  | 207 |  |  | 269 |  |  | 286 |  |  | 244 |
| $16^{\prime}$ |  |  | 193 |  |  | 193 |  |  | 194 |  |  | 252 |  |  | 268 |  |  | 229 |
| 17' | 164 |  | 181 |  |  | 181 |  |  | 183 |  |  | 238 |  |  | 253 |  |  | 216 |
| 18' | 140 |  | 171 | 157 |  | 171 |  |  | 173 | 223 |  | 224 |  |  | 239 |  |  | 204 |
| 19' | 121 |  | 163 | 136 |  | 163 | 152 |  | 164 | 194 |  | 213 | 214 |  | 226 |  |  | 193 |
| 20' | 105 |  | 154 | 118 |  | 154 | 132 |  | 155 | 169 |  | 202 | 186 |  | 215 |  |  | 184 |
| 21' | 92 |  | 147 | 103 |  | 147 | 115 |  | 148 | 148 |  | 193 | 163 |  | 205 | 173 |  | 175 |
| 22' | 80 |  | 136 | 91 |  | 141 | 101 |  | 141 | 130 |  | 184 | 143 |  | 196 | 153 |  | 167 |
| $23 '$ | 71 |  | 124 | 80 |  | 135 | 90 |  | 135 | 115 |  | 176 | 127 |  | 187 | 135 |  | 160 |
| $24^{\prime}$ | 63 |  | 114 | 71 |  | 129 | 80 |  | 130 | 102 |  | 169 | 112 |  | 179 | 120 |  | 153 |
| $25^{\prime}$ | 56 |  | 105 | 63 |  | 124 | 71 |  | 125 | 91 |  | 162 | 100 |  | 172 | 107 |  | 147 |
| 26' | 50 |  | 97 | 56 | 113 | 117 | 63 |  | 120 | 82 |  | 156 | 90 |  | 166 | 96 |  | 142 |
| 27 ' | 45 |  | 90 | 51 | 102 | 108 | 57 | 114 | 115 | 74 | 148 | 150 | 81 |  | 160 | 87 |  | 137 |
| 28 ' | 40 | 81 | 84 | 46 | 92 | 101 | 51 | 103 | 111 | 66 | 133 | 145 | 73 | 146 | 154 | 78 |  | 132 |
| $29^{\prime}$ | 36 | 73 | 78 | 41 | 83 | 94 | 46 | 93 | 107 | 60 | 120 | 140 | 66 | 132 | 149 | 71 |  | 127 |
| 30' | 33 | 66 | 73 | 37 | 75 | 88 | 42 | 85 | 104 | 54 | 109 | 135 | 60 | 120 | 144 | 64 |  | 123 |
| 31' | 30 | 60 | 68 | 34 | 68 | 82 | 38 | 77 | 101 | 50 | 100 | 131 | 54 | 109 | 139 | 59 | 118 | 119 |
| 32' | 27 | 55 | 64 | 31 | 62 | 77 | 35 | 70 | 97 | 45 | 91 | 124 | 49 | 99 | 135 | 53 | 107 | 115 |
| 33' | 25 | 50 | 60 | 28 | 57 | 73 | 32 | 64 | 94 | 41 | 83 | 117 | 45 | 91 | 131 | 49 | 98 | 112 |
| 34' | 23 | 46 | 57 | 26 | 52 | 68 | 29 | 59 | 92 | 38 | 76 | 110 | 41 | 83 | 127 | 45 | 90 | 109 |

## Design Assumptions:

1. Span is the clear distance between supports and is valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The values in the tables are for uniform loads only.
3. Factored Total Load resistance is for standard ( $100 \%$ ) load duration.
4. These tables do not reflect any additional stiffness provided by the sheathing.
5. Live $\mathrm{L} / 360$ Deflection resistance is limited to $\mathrm{L} / 360$. Vibration has not been considered.
6. Total L/180 Deflection resistance is limited to L/180. Long term deflection (creep) has not been considered.
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24."
8. These tables are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least 3-1/2," and are limited to the bearing capacity for an SPF wall plate.

ROOF PITCH ADJUSTMENT FACTORS

| $\begin{array}{l}\text { Roof } \\ \text { Pitch }\end{array}$ | $2: 12$ | $3: 12$ | $4: 12$ | $5: 12$ | $6: 12$ | $7: 12$ | $8: 12$ | $9: 12$ | $10: 12$ | $11: 12$ | $12: 12$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Factor | 1.014 | 1.031 | 1.054 | 1.083 | 1.118 | 1.158 | 1.202 | 1.250 | 1.302 | 1.357 | 1.414 |

## Additional Notes:

1. These tables have been designed to meet the Limit States Design requirements of the National Building Code of Canada.
2. The tabulated resistances represent the capacity of the member in pounds per lineal foot (plf) of length.
3. For roofs with a pitch of $2: 12$ or greater, the horizontal span shall be multiplied by the appropriate pitch adjustment factor from the table at the bottom of this page. Roof joists shall have a minimum pitch of $1 / 4^{" 1}$ per foot (1/4:12) for positive drainage.
4. The designer shall check the Factored Total Load, the Total L/180 Deflection and the Live L/360 Deflection resistance columns.
5. To design for an $\mathrm{L} / 240$ live load deflection, multiply the Live $\mathrm{L} / 360$ Deflection values by 1.5 . To design for a L/480 live load deflection, multiply the Live L/360 Deflection values by 0.75 or refer to the Uniform Floor Load (PLF) Tables on page 10.
6. Where the Deflection resistance is blank, the Factored Total Load resistance governs the design.
7. To design a double 1 -Joist, the values in these tables can be doubled, or the design loads on the $1-$-Joist may be halved to verify the capacity of each ply. The capacity is additive.
8. Web stiffeners are not required for these spans and loads.
9. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require nailing into the web.
10. Do not use a product where designated """ without further analysis by a design professional.

## Roof Span Tables: Low Pitch (6:12 or less) 20, 25 and 30 psf Load

## SPECIFIED ROOF LIVE OR SNOW LOAD (STANDARD DURATION) - 20 PSF ROOF LIVE OR SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" oc |  | 19.2" OC |  | 24" oc |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 18'9" | 18'-5" | 17'-7" | 17'-3" | $16^{\prime}-4$ " | 15'-8" |
|  | 11-7/8" | 22'-8" | 20'11" | 20'-8" | 19'-1" | 18'5" | $17^{\prime \prime} 1^{\prime \prime}$ |
| PWI 20S, LPI 20Plus | 9-1/2" | 20'6" | 20'1' | 19'-3" | 18'-10" | $17^{\prime}-10^{\prime \prime}$ | $17{ }^{\prime \prime}$ " ${ }^{\prime \prime}$ |
|  | 11-7/8" | 24'-7" | 24'-1" | 23'-1" | 22'8" | 21-4" | 20'-3" |
|  | 14 " | 28'1" | 26'11" | 26'5" | $24^{\prime}-7{ }^{\prime \prime}$ | 23'9" | 21-11" |
|  | $16 "$ | 31'-2" | 28-11" | 28'-5" | 26'4" | 25'-5" | 23'6" |
| PWI 32S, LPI 32Plus | 9-1/2" | 21'9" | 21'4" | 20'5" | 20'0" | 18'10" | 18'6" |
|  | 11-7/8" | 26'0" | 25'-5" | 24'-4" | 23-11" | 22'7" | 21-9" |
|  | $14{ }^{\prime \prime}$ | 29'-6" | 28-11" | 27'-9" | 26'-9" | 25'-8" | 23-11" |
|  | $16 "$ | 32'-8" | 31'-8" | 30'-8" | 28-10" | 27-10" | 25'-9" |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 27'-2" | 26'-8" | 25'-6" | 25'0" | 23'-7" | 23'-2" |
|  | 14 " | 30'-9" | $30^{\prime}-2$ " | 28'-11" | 28-4" | 26'-9" | 26'-3" |
|  | $16 "$ | 34'-0" | 33'4" | 31'-11" | 31'-4" | 29'-7" | 27-10" |
| PWI 42S, LPI 42Plus | 9-1/2" | 24'-8" | 24'-2" | 23'-2" | 22'-8" | 21'-5" | 21'0" |
|  | 11-7/8" | 29'-6" | 28-11" | 27'-8" | 27'-2" | 25'-7" | 25'-1" |
|  | 14 " | 33'-6" | 32'-11" | 31'-6" | 30'-10" | 29'-2" | 28-7" |
|  | $16 "$ | $37^{\prime}-2{ }^{\prime \prime}$ | 36'6" | 34'-11" | 34'-3" | $32^{\prime}-4 "$ | 31'-8" |
| PWI 52S, LPI 52Plus | 11-7/8" | $30^{\prime}-6{ }^{\prime \prime}$ | 29'-11" | 28'-8" | 28'1" | $26^{\prime \prime} 6{ }^{\prime \prime}$ | 26'0" |
|  | 14" | 34'-7" | $33^{\prime}-11^{\prime \prime}$ | 32'-6" | 31'-10" | 30'-1" | 29'6" |
|  | $16{ }^{\prime \prime}$ | $38^{\prime}-4{ }^{\prime \prime}$ | $37^{\prime}-7{ }^{\prime \prime}$ | 36'0'0' | 35'-3" | $33^{\prime \prime} 4^{\prime \prime}$ | 32'-8" |
| PWI 56L, LPI 56 | 11-7/8" | $31^{\prime}-6{ }^{\prime \prime}$ | 30'-11" | 29'7" | 29'-0" | 27'-5" | 26'-10" |
|  | $14^{\prime \prime}$ | $35^{\prime}-9$ " | $35^{\prime \prime} 0^{\prime \prime}$ | $33^{\prime}-6{ }^{\prime \prime}$ | 32'-11" | 31'0" | 30'5" |
|  | $16 "$ | 39'-5" | 38'-8" | 37'-0" | $36^{\prime}-4 \prime$ | 34'-3" | $31^{\prime}-2{ }^{\prime \prime}$ |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 25 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" Oc |  | 19.2" oc |  | 24" OC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 17'-4" | 17'-4" | $16^{\prime}-4$ " | $16^{\prime}-4$ " | $15^{\prime \prime} 1^{\prime \prime}$ | 14'-11" |
|  | 11-7/8" | 21'0" | 19'-11" | 19'-3" | 18-2" | 17'-2" | $16^{\prime}-3 "$ |
| PWI 20S, LPI 20Plus | 9-1/2" | 19'-0" | 19'0" | 17'-10" | 17'-10" | 16'-6" | 16'-6" |
|  | 11-7/8" | 22'-9" | 22'9" | 21'-4" | 21-4" | 19'-9" | 19'-4" |
|  | 14 " | 26'0" | 25'-8" | 24'-5" | 23'-5" | 22'-2" | 20'-11" |
|  | $16 "$ | 29'-0" | 27'6" | 26'-7" | 25'-1" | 23-9" | 22'-5" |
| PWI 32S, LPI 32Plus | 9-1/2" | 20'-1' | 20'1" | 18'-10" | 18'-10" | 17'-5" | 17'-5" |
|  | 11-7/8" | 24'-0" | 24'0" | 22'7" | 22'-7" | 20'10" | 20'9" |
|  | 14 " | 27'-4" | $27^{\prime \prime} 4^{\prime \prime}$ | 25'-8" | $25^{\prime}$-6" | 23'9" | 22'9" |
|  | $16 "$ | 30'-3" | 30'-2' | 28'5" | 27'-6" | 26'0" | 23'8" |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 25'-2" | 25'-2" | 23'-7" | 23'-7" | 21'10" | 21'-10" |
|  | $14^{\prime \prime}$ | 28'-6" | 28'6" | 26'-9" | 26'-9" | 24'-9" | 24'-9" |
|  | $16 "$ | 31'-6" | 31'6" | 29'-7" | 29'-7" | 27-4" | 25'0" |
| PWI 42S, LPI 42Plus | 9-1/2" | 22'-10" | 22'-10" | 21'-5" | 21'-5" | 19'-10" | 19'-10" |
|  | 11-7/8" | 27'-4" | 27'-4" | 25'-7" | 25'-7" | 23'8" | 23'8" |
|  | $14 "$ | $31^{\prime \prime} \mathbf{1 ' ~}^{\prime \prime}$ | 31'-1" | 29'-2" | 29'-2" | 27-0" | 27-0" |
|  | $16 "$ | 34'-5" | 34'-5" | 32'-4" | $32^{\prime}-4 "$ | 29-11" | 29'-11" |
| $\begin{aligned} & \text { PWI 52S, } \\ & \text { LPI 52Plus } \end{aligned}$ | 11-7/8" | 28'-3" | 28'3" | 26'6" | 26'6" | 24'6" | 24'-6" |
|  | $14{ }^{\prime \prime}$ | $32^{\prime}-0^{\prime \prime}$ | $32^{\prime} \cdot 01$ | $30^{\prime}-1$ " | $30^{\prime}-1$ " | 27-10" | 27-10" |
|  | $16 "$ | 35'-6" | $35^{\prime \prime}$ " | $33^{\prime \prime} \mathbf{4}^{\prime \prime}$ | $33^{\prime}-4 "$ | $30^{\prime}-10^{\prime \prime}$ | 30'-10" |
| PWI 56L, LPI 56 | 11-7/8" | 29'-2" | 29'-2" | 27'-5" | 27'-5" | 25'4" | 25'4" |
|  | $14^{\prime \prime}$ | 33'-1" | 33'1" | 31'-0" | 31'-0" | 28-9" | 28-2" |
|  | $16 "$ | 36'-6" | $36^{\prime \prime}$ " | $34^{\prime}-3 "$ | $34^{\prime}-3 \prime \prime$ | 31'-8" | 28'3" |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 30 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" OC |  | 19.2" oc |  | 24" OC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | $16^{\prime}-4$ " | 16'4" | 15'-4" | 15'-4" | 14'-2" | 14'-1' |
|  | 11-7/8" | 19'-8" | 18-11" | 18'-1' | 17'-3" | 16'-2" | 15'-4" |
| PWI 20S, LPI 20Plus | 9-1/2" | 17-10" | 17'-10" | 16'8" | 16'-8" | 15'5" | 15'-5" |
|  | 11-7/8" | 21-4" | 21-4" | 20'1' | 20'-1" | 18'6" | 18'-3" |
|  | 14 | 24'-5" | 24'3" | 22'-11" | 22'-2" | 20'-10" | 19'-9" |
|  | $16^{\prime \prime}$ | 27'-2" | 26'0" | 25'0" | 23'-9" | 22'4" | 21'-3" |
| PWI 32S,LPI 32Plus | 9-1/2" | 18-10" | 18-10" | 17'-8" | 17'-8" | 16'4" | 16'4" |
|  | 11-7/8" | 22'-7" | 22'-7" | 21-2" | 21'-2" | 19'7" | 19'-7" |
|  | 14 | 25'8" | 25'-8" | 24'-1" | 24'-1" | 22'-3" | 21'-2" |
|  | $16^{\prime \prime}$ | 28'5" | 28'5" | 26'8" | 26'0" | 23'-6" | 21'-3" |
| $\begin{gathered} \text { PWI 36L, } \\ \text { LPI } 36 \end{gathered}$ | 11-7/8" | 23'7" | 23'7" | 22-2" | 22'-2" | 20'6" | 20'6" |
|  | 14 " | 26'-9" | 26'-9" | 25'1'1' | 25'-1" | 23'3" | 22'-3" |
|  | 16" | 29'-7" | 29'-7" | 27'-9" | 27'-9" | 24'-6" | 22'3" |
| PWI 42S, LPI 42Plus | 9-1/2" | 21'-5" | 21'-5" | $20^{-1} \mathbf{1}^{\prime \prime}$ | $20^{-1} \mathbf{1}^{\prime \prime}$ | 18'7" | $18^{\prime}$-7" |
|  | 11-7/8" | 25'-7" | 25'-7" | 24'0" | $24^{\prime}-0^{\prime \prime}$ | 22'3" | 22'3" |
|  | $14^{\prime \prime}$ | 29'-2" | 29'-2" | $27^{\prime}-4 \prime$ | $27^{\prime}-4{ }^{\prime \prime}$ | 25-4" | $25^{\prime \prime} \mathbf{4}^{\prime \prime}$ |
|  | $16 "$ | $32^{\prime}-4$ " | $32^{\prime}-4$ " | $30^{\prime}-4^{\prime \prime}$ | $30^{\prime}-4^{\prime \prime}$ | 28-1" | 28-1" |
| PWI 52S, LPI 52Plus | 11-7/8" | 26'6" | 26'-6" | 24'-11" | 24'-11" | 23'0" | 23'0" |
|  | 14" | 30'-1" | 30'-1" | 28'-3" | 28'-3" | 26'-2" | 26'2" |
|  | $16^{\prime \prime}$ | $33^{\prime \prime} 4^{\prime \prime}$ | $33^{\prime \prime} 4^{\prime \prime}$ | 31'-3" | $31^{\prime}-3{ }^{\prime \prime}$ | 28'-11" | 28-11" |
| PWI 56L, LPI 56 | 11-7/8" | 27'-5" | 27'-5" | 25'-8" | 25'-8" | 23'-9" | 23'-9" |
|  | 14" | 31'-0" | $31^{\prime}-0 \mid 1$ | 29'-2" | 29'-2" | 26'-11" | 25'-3" |
|  | $16^{\prime \prime}$ | 34'-3" | 34'-3" | $32^{\prime}-2{ }^{\prime \prime}$ | 31'-9" | 28'-0" | 25'4" |

Table Usage:

1. Select the appropriate set of tables based on roof pitch.
2. Select the section of that table that corresponds to the specified roof live or snow load.
3. Find a span that meets or exceeds the design span for the appropriate specified roof dead load ( 15 psf or 20 psf).
4. Read the corresponding series, depth and spacing.

Design Assumptions:

1. The spans listed are the horizontal clear distance between supports and are valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform gravity loads only as listed for each table, including the effects of a 300 lb concentrated load. These spans have not been evaluated for wind.
3. These tables do not reflect any additional stiffness provided by the roof sheathing.
4. Live load deflection is limited to $\mathrm{L} / 360$.
5. Total load deflection is limited to $\mathrm{L} / 180$.
6. The spans are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing capacity for an SPF wall plate.
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24 "

Additional Notes:

1. Web stiffeners are not required for the Roof Span tables except when using a "bird's mouth" detail for the low-end bearing.
2. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require nailing into the web.
3. L/360 represents the maximum deflection allowed per code for roof joists supporting plaster or gypsum ceilings. Verify deflection limits with local code requirements.
4. Roof joists must have a minimum pitch of $1 / 4$ " per foot (1/4:12) for positive drainage.
5. Roof applications in high wind areas require special analysis which may reduce spans and may require bracing of the bottom flange and special connectors to resist uplift.
6. For conditions not shown, use the Uniform Roof Load (PLF) tables, use the Exacte by PWT software or contact your PWT ${ }^{\text {mw }}$ distributor for assistance.


ACTUAL DEFLECTION BASED ON SPAN AND LIMIT

| Span (ft) | L/360 | L/240 | L/180 |
| :---: | :---: | :---: | :---: |
| 10' | 5/16" | 1/2" | 11/16" |
| 12 | 3/8" | 5/8" | 13/16" |
| $14^{\prime}$ | 7/16" | 11/16" | 15/16" |
| $16^{\prime}$ | 9/16" | 13/16" | 1-1/16" |
| $18{ }^{\prime}$ | 5/8" | 7/8" | 1-3/16" |
| $20^{\prime}$ | 11/16" | $1{ }^{\prime \prime}$ | 1-5/16" |
| 22 | 3/4" | 1-1/8" | 1-7/16" |
| $24^{\prime}$ | 13/16" | 1-3/16" | 1-5/8" |
| $26^{\prime}$ | 7/8" | 1-5/16" | 1-3/4" |
| $28^{\prime}$ | 15/16" | 1-3/8" | 1-7/8" |
| 30' | 1" | 1-1/2" | $2 "$ |

* Deflections rounded to the nearest $1 / 16 . "$


## Roof Span Tables: Low Pitch (6:12 or less) 40,50 and 60 psf Load

## SPECIFIED SNOW LOAD (STANDARD DURATION) - 40 PSF SNOW

| Series Specified | $\text { Dead Load } \rightarrow$ | 16" OC |  | 19.2" oc |  | 24" OC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 14'-9" | 14'-9" | 13'-10" | 13'-10" | $12^{\prime}$ '9" | 12'-9" |
|  | 11-7/8" | 17'-10" | 17'-2' | $16^{\prime}-4 "$ | $15^{\prime}-8$ " | 14'-7" | 14-0" |
| PWI 20S, LPI 20Plus | 9-1/2" | 16'-1' | $16^{-1} \mathbf{1}^{\prime \prime}$ | $15^{\prime \prime}$-1" | $15^{\prime}-1{ }^{\prime \prime}$ | 13-11" | 13'-11" |
|  | 11-7/8" | 19'-4" | 19'-4" | 18'-1" | 18'-1" | 16'-9" | 16'7" |
|  | 14 | 22'1" | 22'-1' | 20'9" | 20'2" | 18-9" | $17^{\prime}-6 "$ |
|  | $16 "$ | $24^{\prime}-7{ }^{\prime \prime}$ | 23'8" | 22'6" | 21'7" | 19'-1" | $17^{\prime \prime} 7^{\prime \prime}$ |
| PWI 32S, <br> LPI 32Plus | 9-1/2" | $17^{\prime}-1{ }^{\prime \prime}$ | 17-1' | $16^{\prime}-0{ }^{\prime \prime}$ | $16^{\prime}-0{ }^{\prime \prime}$ | $14{ }^{\prime}-9$ " | $14^{\prime}-9$ " |
|  | 11-7/8" | 20'5" | 20'5" | 19'-1" | 19'-1" | 17'8" | 17'-1" |
|  | $14{ }^{\prime \prime}$ | 23'-2" | 23'2" | 21'-9" | 21'-9" | 19'0" | $17^{\prime \prime}$ " ${ }^{\prime \prime}$ |
|  | $16 "$ | 25'-8" | 25'-8" | 23-11" | 22'0" | 19'-1" | $17^{\prime \prime}-7{ }^{\prime \prime}$ |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 21'4" | 21-4" | 20'0" | 20'0" | 18'-6" | 18-4" |
|  | 14 " | 24'-2" | 24'2" | 22'-8" | 22'-8" | 19'9" | 18'-4" |
|  | $16 "$ | 26'-9" | 26'-9" | 24'-9" | 22'-11" | 19'9" | 18'-4" |
| PWI 42S, LPI 42Plus | 9-1/2" | 19'-4" | 19'-4" | 18'-2" | 18'2" | 16'9" | 16'9" |
|  | 11-7/8" | 23'-2" | 23'2" | 21'-9" | 21'-9" | 20'1" | 20'1" |
|  | $14 "$ | 26'4" | 26'4" | 24'-9" | 24'-9" | 22-10" | 22'-10" |
|  | $16 "$ | 29'-3" | 29'-3" | 27'-5" | 27'-5" | 25'4" | 23-10" |
| PWI 52S,LPI 52Plus | 11-7/8" | 24'-0" | 24'-0" | 22'-6" | 22'-6" | 20'10" | 20'10" |
|  | 14" | 27'3" | 27'-3" | 25'7" | 25'7" | 23'-8" | 23'-8" |
|  | $16{ }^{\prime \prime}$ | 30'-2" | 30'2" | 28'-4" | 28'-4" | 26'2" | 25'-4" |
| PWI 56L, LPI 56 | 11-7/8" | 24'-9" | 24-9" | 23'3" | 23'3" | 21'-6" | 20'10" |
|  | $14^{\prime \prime}$ | 28'-1" | 28'1' ${ }^{\prime \prime}$ | 26'4" | 26'-2" | 22'-9" | 20'-11" |
|  | $16 "$ | $31^{\prime}-0 "$ | 31'0" | 28-7" | 26'-3" | 22'-9" | 20'-11" |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 50 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" oc |  | 19.2" OC |  | 24" oc |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 13'-8" | 13'-8" | 12'-9" | 12'-9" | 11'10" | 11'-10" |
|  | 11-7/8" | 16'-5" | 15'-10" | 15'0" | $14^{\prime}-5 "$ | $13^{\prime}-4$ " | 12-11" |
| PWI 20S, LPI 20Plus | 9-1/2" | 14'-10" | 14'-10" | 13'11" | 13'11" | 12'-10" | 12'-10" |
|  | 11-7/8" | 17-10" | 17'-10" | 16'-9" | 16'-9" | 15'-5" | 14'-6" |
|  | 14 " | 20'5" | 20'5" | 19'-2" | 18'7" | 16'0" | 14'-11" |
|  | $16 "$ | 22'-8" | 21'-11" | 20'-2" | 18'9" | $16^{\prime}-1$ " | 14'-11" |
| PWI 32S,LPI 32Plus | 9-1/2" | 15'-9" | 15'9" | $14{ }^{\prime}-9 "$ | $14^{\prime}-9 "$ | 13'-8" | $13^{\prime \prime} \mathbf{7}^{\prime \prime}$ |
|  | 11-7/8" | 18-10" | 18'10" | $17^{\prime \prime}$-8 | $17^{\prime \prime}-8$ | 15'-5" | 14'-6" |
|  | 14 " | 21'5" | 21'5" | 20'-1" | 18'8" | 16'0" | 14'-11" |
|  | $16 "$ | 23'-9" | 22'-7" | 20'-2' | 18'-9" | $16^{\prime}-1{ }^{\prime \prime}$ | 14-11" |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 19'9" | 19'9" | 18'-6" | $18^{\prime}-6{ }^{\prime \prime}$ | 16'-7" | 15'-6" |
|  | $14^{\prime \prime}$ | 22'-5" | 22'-5" | 20'-9" | 19'-5" | 16'7" | 15'-6" |
|  | $16^{\prime \prime}$ | 24'-9" | 23'5" | 20'-9" | 19'-5" | 16'7" | $15 ' 6 "$ |
| PWI 42S, LPI 42Plus | 9-1/2" | 17'-11" | 17'-11" | 16'-9" | 16'-9" | 15'-6" | 15 '6" |
|  | 11-7/8" | 21'-5" | 21'5" | 20'1" | 20'1" | 18'6" | 18'6" |
|  | $14{ }^{\prime \prime}$ | 24'-5" | 24'-5" | 22-10" | 22-10" | 20'11" | 19'7" |
|  | $16 "$ | 27-1" | 27-1" | $25^{\prime}-4 "$ | 25'4" | 21'7" | 20'3" |
| PWI 52S, LPI 52Plus | 11-7/8" | 22'-2" | 22'-2" | 20'10" | 20'10" | 19'3" | 19'3" |
|  | $14^{\prime \prime}$ | 25'-2" | 25'-2" | 23'8" | 23'8" | 21'10" | 21'5" |
|  | $16 "$ | 27-11" | 27-11" | 26'-2" | 26'-2" | 23'0" | 21'6" |
| PWI 56L, LPI 56 | 11-7/8" | 22-11" | 22'-11" | 21'6" | 21'6" | 19'1" | 17'-9" |
|  | $14^{\prime \prime}$ | 26'0" | 26'0" | $24^{\prime}-0{ }^{\prime \prime}$ | 22'-4" | 19'-2" | 17-10" |
|  | $16 "$ | 28-8" | 26'-11" | $24^{\prime}-0$ " | $22^{\prime \prime}-5$ | 19'-2" | 17-10" |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 60 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" Oc |  | 19.2" oc |  | 24" oc |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 12'-9" | 12'9" | $12^{\prime}-0^{\prime \prime}$ | 12'0" | 11'1" | $10^{\prime}-7{ }^{\prime \prime}$ |
|  | 11-7/8" | 15'-3" | 14'-10" | 13-11" | 13'6" | 11-11" | 11'-3" |
| PWI 20S, LPI 20Plus | 9-1/2" | 13'11" | 13'11" | 13'-1" | $13^{\prime \prime} 1{ }^{\prime \prime}$ | $12^{\prime}-0$ " | 11-10" |
|  | 11-7/8" | 16'9" | 16'9" | 15'-8" | 15'-8" | 13'-3" | 12'7" |
|  | 14 | 19'-2" | 19'-1" | $17^{\prime \prime}-4$ | $16^{\prime}-3 "$ | 13 '9" | 12'-11" |
|  | $16 "$ | 20-11" | 19'-8" | $17^{\prime \prime}-5{ }^{\prime \prime}$ | $16^{\prime}-4$ " | 13-10" | $13^{\prime}-0^{\prime \prime}$ |
| PWI 32S, LPI 32Plus | 9-1/2" | 14-9" | $14^{\prime}-9$ " | 13'-10" | 13'10" | $12^{\prime}-6 "$ | 11'-10" |
|  | 11-7/8" | $17^{\prime \prime}$-8' | $17^{\prime \prime}-8$ | $16^{\prime}-7{ }^{\prime \prime}$ | 15'9" | 13'-3" | 12'7" |
|  | 14 " | 20'-1" | 19'7" | $17^{\prime \prime}-4$ | $16^{\prime}-3 "$ | 13 -9" | 12-11" |
|  | $16{ }^{\prime \prime}$ | 20'11" | 19'-8" | $17^{\prime \prime}-5{ }^{\prime \prime}$ | $16^{\prime}-4^{\prime \prime}$ | 13'10" | 13'0" |
| $\begin{gathered} \text { PWI 36L, } \\ \text { LPI 36, } \end{gathered}$ | 11-7/8" | 18'6" ${ }^{\prime \prime}$ | 18'-6" | 17'-4" | 16'-11" | 14'-3" | 13'-5" |
|  | $14^{\prime \prime}$ | 21'0" | 20'4" | 17'-10" | 16'-11" | 14'3" | 13'-5" |
|  | $16 "$ | 21'-6" | 20'4" | 17'-10" | 16'-11" | 14'3" | 13'-5" |
| PWI 42S, LPI 42Plus | 9-1/2" | 16'9" | 16'9" | 15'-8" | 15'-8" | $14^{\prime}-6 "$ | 14'-6" |
|  | 11-7/8" | 20'1" | 20'1" | 18'-10" | 18-10" | $17^{\prime \prime}-4$ | 16'-4" |
|  | 14" | 22-10" | 22'10" | 21'5" | 21-4" | 18'0" | $17^{\prime}-0{ }^{\prime \prime}$ |
|  | $16 "$ | 25'-4" | 25'-4" | 23'3" | 22'0" | 18'7" | $17^{\prime}-7{ }^{\prime \prime}$ |
| PWI 52S,LPI 52Plus | 11-7/8" | 20'-10" | 20'-10" | 19'-6" | 19'6" | 18'0" | 18'0" |
|  | $14^{\prime \prime}$ | 23'8" | 23'8" | 22'-2" | 22'-2" | 19'-8" | 18'7" |
|  | $16 "$ | 26'2" | 26'-2" | 24'-7" | 23'-5" | 19'9" | 18'8" |
| $\begin{gathered} \text { PWI 56L, } \\ \text { LPI } 56 \end{gathered}$ | 11-7/8" | 21'6" | 21'6" | 20'1" | 19'-5" | 16'6" | 15'-6" |
|  | $14^{\prime \prime}$ | 24'-4" | 23'-5" | 20'8" | 19'-5" | 16'-6" | $15 ' 6 "$ |
|  | $16 "$ | 24-11" | 23'-5" | 20'-9" | 19'-6" | $16^{\prime}-6 "$ | $15 ' 6 "$ |

Table Usage:

1. Select the appropriate set of tables based on roof pitch
2. Select the section of that table that corresponds to the specified roof live or snow load.
3. Find a span that meets or exceeds the design span for the appropriate specified roof dead load ( 15 psf or 20 psf).
4. Read the corresponding series, depth and spacing.

## Design Assumptions:

1. The spans listed are the horizontal clear distance between supports and are valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform gravity loads only as listed for each table, including the effects of a 300 lb concentrated load. These spans have not been evaluated for wind.
3. These tables do not reflect any additional stiffness provided by the roof sheathing.
4. Live load deflection is limited to $\mathrm{L} / 360$.
5. Total load deflection is limited to $\mathrm{L} / 180$.
6. The spans are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing capacity for an SPF wall plate.
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24 "

Additional Notes:

1. Web stiffeners are not required for the Roof Span tables except when using a "birrd's mouth" detail for the low-end bearing.
2. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require nailing into the web.
3. $\mathrm{L} / 360$ represents the maximum deflection allowed per code for roof joists supporting plaster or gypsum ceilings. Verify deflection limits with local code requirements.
4. Roof joists must have a minimum pitch of $1 / 4$ " per foot (1/4:12) for positive drainage.
5. Roof applications in high wind areas require special analysis which may reduce spans and may require bracing of the bottom flange and special connectors to resist uplift.
6. For conditions not shown, use the Uniform Roof Load (PLF) tables, use the Exacte by PWT software or contact your PWT ${ }^{\text {mu }}$ distributor for assistance.


ACTUAL DEFLECTION BASED ON SPAN AND LIMIT

| Span (ft) | L/360 | L/240 | L/180 |
| :---: | :---: | :---: | :---: |
| 10' | 5/16" | 1/2" | 11/16" |
| $12 '$ | 3/8" | 5/8" | 13/16" |
| $14^{\prime}$ | 7/16" | 11/16" | 15/16" |
| $16^{\prime}$ | 9/16" | 13/16" | 1-1/16" |
| $18{ }^{\prime}$ | 5/8" | 7/8" | 1-3/16" |
| 20' | 11/16" | 1" | 1-5/16" |
| $22^{\prime}$ | 3/4" | 1-1/8" | 1-7/16" |
| $24^{\prime}$ | 13/16" | 1-3/16" | 1-5/8" |
| $26^{\prime}$ | 7/8" | 1-5/16" | 1-3/4" |
| $28^{\prime}$ | 15/16" | 1-3/8" | 1-7/8" |
| 30' | $1^{\prime \prime}$ | 1-1/2" | $2{ }^{\prime \prime}$ |

[^0]
## Roof Span Tables: High Pitch (6:12 to 12:12) 20, 25 and 30 psf Load

SPECIFIED ROOF LIVE OR SNOW LOAD (STANDARD DURATION) - 20 PSF ROOF LIVE OR SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" OC |  | 19.2" OC |  | 24"0c |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 17'-3" | 16'4" | $16^{-2}{ }^{\prime \prime}$ | 15-4" | $15^{-0} 0^{\prime \prime}$ | 14'2" |
|  | 11-7/8" | 20'-9" | 19'2" | 19'-6" | 17'-6" | 17'-5" | $15 ' 7{ }^{\prime \prime}$ |
| PWI 20S, LPI 20Plus | 9-1/2" | 18-10" | 17'-10" | 17'-8" | 16'-9" | 16'-4" | 15'-6" |
|  | 11-7/8" | 22'-7" | 21'5" | 21'-2" | 20'-1' | 19'-8" | 18'7" |
|  | 14 | 25-10" | 24'-5" | 24'-3" | 22'-6" | 22'-4" | 20'1" |
|  | $16 "$ | 28-9" | 26'-5" | 26'-10" | 24'-2" | 24'0" | 21'7" |
| PWI 32S,LPI 32Plus | 9-1/2" | 19'-11" | 18'11" | 18'9" | 17'-9" | 17'-4" | 16'-5" |
|  | 11-7/8" | 23-10" | 22'7" | 22'5" | 21'-2" | 20'9" | 19'-8" |
|  | 14 | 27-1" | 25'-8" | 25'-6" | 24'-1' | 23'7" | 21-10" |
|  | $16 "$ | 30'0" | 28'5" | 28'-2" | 26'-5" | 26'1" | 21'-11" |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 24'-11" | 23'-8" | 23'-5" | 22'-2" | 21'-8" | 20'7" |
|  | $14^{\prime \prime}$ | 28'-3" | 26'9" | 26'-7" | 25'-2" | 24'-7" | 23'3" |
|  | $16 "$ | 31'-3" | 29'-7" | 29'4" | 27'-9" | 27'-2" | 23'-4" |
| PWI 42S, LPI 42Plus | 9-1/2" | 22'-8" | 21'-5" | 21'-3" | 20'-1' | 19'-8" | 18'8" |
|  | 11-7/8" | 27-1" | 25'8" | 25'-5" | 24'-1" | 23'-7" | 22'4" |
|  | $14^{\prime \prime}$ | 30'-9" | 29'-2" | 28-11" | 27'-5" | 26'10" | $25^{\prime}-4$ " |
|  | $16 "$ | 34'-2" | $32^{\prime}-4 "$ | 32'1" | 30'-5" | 29'-9" | 28-2" |
| PWI 52S,LPI 52Plus | 11-7/8" | 28'0" | 26'6" | 26'-3" | 24'-11" | 24'-4" | 23'-1" |
|  | 14 " | 31'-9" | $30^{\prime}-1$ " | 29'-10" | 28'-3" | 27'-8" | 26'-2" |
|  | $16 "$ | 35'-2" | $33^{\prime \prime} \mathbf{4}^{\prime \prime}$ | 33'0" | 31'-3" | $30^{\prime}-7{ }^{\prime \prime}$ | 29'0" |
| PWI 56L, LPI 56 | 11-7/8" | 28'11" | 27'-5" | 27'-2" | 25'-9" | 25'-2" | 23'10" |
|  | 14 " | 32'-10" | 31'-1" | 30'-10" | 29'-2" | 28'-6" | 26'1" |
|  | $16 "$ | 36'-3" | $34^{\prime}-4 "$ | 34'-0" | 32'-3" | 31'-6" | 26'-2" |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 25 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" oc |  | 19.2" oc |  | 24" OC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 16'1" | 15'9" | 15'2" | 14'-10" | 14'0" | 13'-8" |
|  | 11-7/8" | 19'-5" | 18'8" | 18'-3" | $17^{\prime}-0{ }^{\prime \prime}$ | $16^{\prime}-5{ }^{\prime \prime}$ | 15'-2" |
| PWI 20S, LPI 20Plus | 9-1/2" | 17'-7" | 17'-3" | 16'6" | $16^{\prime}-2{ }^{\prime \prime}$ | 15'-4" | 15'0" |
|  | 11-7/8" | 21'1' | 20'8" | 19'-10" | 19'-5" | 18'-4" | 18'0" |
|  | $14 "$ | 24'-2" | 23'-8" | 22'-8" | 21'10" | 21'-0" | 19'-6" |
|  | $16 "$ | 26'-11" | 25'8" | 25'-3" | 23'-5" | 22'-8" | 20'8" |
| PWI 32S, LPI 32Plus | 9-1/2" | 18'8'8 | 18'-3" | 17'-6" | 17'-2" | 16'3" | 15 -10" |
|  | 11-7/8" | 22'-4" | 21'10" | 20'-11" | 20'6" | 19'5" | 19'0" |
|  | 14 " | 25'-4" | 24'-10" | 23'10" | 23'4" | 22'-1" | 20'7" |
|  | $16 "$ | 28'-1' | 27'-6" | 26'5" | 25'-8" | 24'-3" | 20'8" |
| $\begin{gathered} \text { PWI 36L, } \\ \text { LPI } 36 \end{gathered}$ | 11-7/8" | 23'-4" | 22'-10" | 21'-11" | 21'5" | 20'-4" | 19'-10" |
|  | $14^{\prime \prime}$ | 26'6" | 25'-11" | 24'-10" | 24'-4" | 23'-0" | 21'11" |
|  | $16^{\prime \prime}$ | 29'-3" | 28'7" | 27'-5" | 26'10" | 25'-5" | 22'0" |
| PWI 42S, LPI 42Plus | 9-1/2" | 21'-2" | 20'-9" | 19'-11" | 19'-5" | 18'5" | 18'0" |
|  | 11-7/8" | 25'-4" | 24'9" | 23'10" | 23'-3" | 22'-0" | 21'7" |
|  | $14{ }^{\prime \prime}$ | 28-10" | 28'2" | 27'-1' | 26'6" | 25'1" | 24 '6" |
|  | $16^{\prime \prime}$ | 32'0" | 31'-3" | 30'-0" | 29'-5" | 27'-10" | 27-2" |
| PWI 52S,LPI 52Plus | 11-7/8" | 26'-2" | 25'7" | 24'-7" | 24'-1" | 22'-9" | 22'3" |
|  | 14 " | 29'-9" | 29'-1" | 27-11" | $27^{\prime \prime}-4{ }^{\prime \prime}$ | 25'-10" | 25'4" |
|  | $16^{\prime \prime}$ | 32'-11" | $32^{\prime}-2{ }^{\prime \prime}$ | 30'-11" | 30'-3" | 28'-8" | 28'0" |
| PWI 56L, LPI 56 | 11-7/8" | 27'-1" | 26'6" | 25'5" | 24'-11" | 23'7" | 23'1" |
|  | $14^{\prime \prime}$ | 30'-8" | $30^{\prime}-0^{\prime \prime}$ | 28'10" | 28'-2" | 26'-8" | 24'-7" |
|  | $16^{\prime \prime}$ | 33'-11" | 33'-2" | 31'-10" | $30^{\prime}-11^{\prime \prime}$ | 28-11" | $24^{\prime}-8 "$ |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 30 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" OC |  | 19.2" oc |  | 24" oc |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | $15^{\prime}-2$ " | 15'-2" | $14^{\prime}$-3" | $14^{\prime}-3$ " | $13^{\prime}-2$ " | 13'2" |
|  | 11-7/8" | 18'-3" | 18'0" | $17^{\prime \prime} 2^{\prime \prime}$ | $16^{\prime}-5 "$ | $15^{\prime}-6 "$ | $14^{\prime}-8$ " |
| PWI 20S, LPI 20Plus | 9-1/2" | 16'-6" | $16^{\prime}-6{ }^{\prime \prime}$ | 15 '6" | $15 ' 6 "$ | $14^{\prime}-4$ " | $14^{\prime \prime} \mathbf{4}^{\prime \prime}$ |
|  | 11-7/8" | 19'10" | 19'10" | 18'-8" | 18'-8" | $17^{\prime \prime}-3$ | $17^{\prime \prime}-3$ " |
|  | 14 " | 22'-8" | 22'-8" | 21'-4" | 21'1" | 19'-9" | 18'10" |
|  | $16 "$ | 25'-3" | 24-10" | 23'9" | 22'-7" | 21'-5" | 19'3" |
| PWI 32S, LPI 32Plus | 9-1/2" | 17'-6" | 17'-6" | $16^{\prime}-6 "$ | $16^{\prime}-6{ }^{\prime \prime}$ | 15'-3" | 15'-3" |
|  | 11-7/8" | 20'11" | 20'11" | 19'-8" | 19'-8" | 18'-2" | 18'-2" |
|  | 14 | 23-10" | 23-10" | 22'-4" | 22'-4" | 20'-8" | 19'-2" |
|  | $16^{\prime \prime}$ | 26'-5" | 26'5" | 24'-9" | 24'-2" | 21'-8" | 19'-3" |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 21-11" | 21'11" | 20'7" | 20'7" | 19'-1" | 19'-1" |
|  | 14" | 24'-10" | 24'-10" | 23'4" | 23'4" | 21'7" | 20'5" |
|  | $16 "$ | 27'-5" | 27'-5" | 25'-9" | 25'-8" | 23-1" | 20'6" |
| PWI 42S, LPI 42Plus | 9-1/2" | 19'-11" | 19'-11" | 18'8" | $18^{\prime}-8{ }^{\prime \prime}$ | $17^{\prime \prime}-3 "$ | 17'-3" |
|  | 11-7/8" | 23-10" | 23-10" | 22'-4" | 22'-4" | 20'8" | 20'-8" |
|  | $14^{\prime \prime}$ | 27'-1" | 27'-1' | 25'-5" | 25'-5" | 23'6" | 23'6" |
|  | $16 "$ | 30'0" | 30'0" | 28'-2" | 28'-2" | 26'1" | 26'1" |
| PWI 52S, LPI 52Plus | 11-7/8" | 24'-7" | 24'-7" | 23'1" | 23'1" | 21'5" | 21'5" |
|  | 14 " | 27-11" | 27-11" | 26'-3" | 26'-3" | 24'-3" | 24'-3" |
|  | $16^{\prime \prime}$ | 30'-11" | 30'-11" | 29'0" | 29'0" | 26-11" | 26-11" |
| PWI 56L, LPI 56 | 11-7/8" | 25'5" | 25'5" | 23-11" | 23-11" | 22'-1" | 22'-1" |
|  | $14^{\prime \prime}$ | 28-10" | 28'10" | 27'-1" | 27-1" | 25'1" | 22'-11" |
|  | $16 "$ | 31'-10" | 31'-10" | 29'-11" | 28'9" | 25'10" | 22'-11" |

Table Usage:

1. Select the appropriate set of tables based on roof pitch.
2. Select the section of that table that corresponds to the specified roof live or snow load.
3. Find a span that meets or exceeds the design span for the appropriate specified roof dead load ( 15 pst or 20 psf).
4. Read the corresponding series, depth and spacing.

Design Assumptions:

1. The spans listed are the horizontal clear distance between supports and are valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform gravity loads only as listed for each table, including the effects of a 300 lb concentrated load. These spans have not been evaluated for wind.
3. These tables do not reflect any additional stiffness provided by the roof sheathing.
4. Live load deflection is linited to $L / 360$.
5. Total load deflection is limited to $\mathrm{L} / 180$.
6. The spans are based on an end bearing lensth of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$, " and are limited to the bearing capacity for an SPF wall plate.
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24 ".

Additional Notes:

1. Web stiffeners are not required for the Roof Span tables except when using a "bird's mouth" detail for the low-end bearing.
2. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require nailing into the web.
3. $L / 360$ represents the maximum deflection allowed per code for roof joists supporting plaster or gypsum ceilings. Verify deflection limits with local code requirements.
4. Roof joists must have a minimum pitch of $1 / 4$ " per foot (1/4:12) for positive drainage.
5. Roof applications in high wind areas require special analysis which may reduce spans and may require bracing of the bottom flange and special connectors to resist uplift.
6. For conditions not shown, use the Uniform Roof Load (PLF) tables, use the Exacte by PWT software or contact your PWT" distributor for assistance.


ACTUAL DEFLECTION BASED ON SPAN AND LIMIT

| Span (ft) | L/360 | L/240 | L/180 |
| :---: | :---: | :---: | :---: |
| $10^{\prime}$ | 5/16" | 1/2" | 11/16" |
| $12^{\prime}$ | 3/8" | 5/8" | 13/16" |
| $14{ }^{\prime}$ | 7/16" | 11/16" | 15/16" |
| $16^{\prime}$ | 9/16" | 13/16" | 1-1/16" |
| $18{ }^{\prime}$ | 5/8" | 7/8" | 1-3/16" |
| $20^{\prime}$ | 11/16" | $1{ }^{1 \prime}$ | 1-5/16" |
| $22^{\prime}$ | 3/4" | 1-1/8" | 1-7/16" |
| $24^{\prime}$ | 13/16" | 1-3/16" | $1-5 / 8^{\prime \prime}$ |
| $26^{\prime}$ | 7/8" | 1-5/16" | 1-3/4" |
| $28^{\prime}$ | 15/16" | 1-3/8" | 1-7/8" |
| $30^{\prime}$ | 1" | $1-1 / 2^{\prime \prime}$ | $2 "$ |

[^1]
## Roof Span Tables: High Pitch (6:12 to 12:12) 40,50 and 60 psf Load

## SPECIFIED SNOW LOAD (STANDARD DURATION) - 40 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" OC |  | 19.2" OC |  | 24" OC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 13'-8" | 13'-8" | 12'-10" | 12'-10" | 11'11" | 11'-11" |
|  | 11-7/8" | 16'6" | 16'6" | $15 ' 6 "$ | $15^{\prime}-0{ }^{\prime \prime}$ | 14'-1" | 13'5" |
| PWI 20S, LPI 20Plus | 9-1/2" | 14'-11" | 14'-11" | $14^{\prime}-0$ " | $14^{\prime}-0$ " | $13^{\prime}-0{ }^{\prime \prime}$ | 13'0" |
|  | 11-7/8" | $17^{\prime}-11^{\prime \prime}$ | $17^{\prime}-11^{\prime \prime}$ | $16^{\prime}-10^{\prime \prime}$ | 16-10" | 15'-7" | 15'7" |
|  | 14 | 20'7" | 20'7" | 19'-3" | 19'-3" | 17'-9" | 16'1" |
|  | $16 "$ | 22-10" | 22'9" | 21'6" | 20'3" | 17-10" | $16^{\prime}-2$ " |
| PWI 32S, LPI 32Plus | 9-1/2" | $15^{\prime}-10^{\prime \prime}$ | $15^{\prime}-10^{\prime \prime}$ | $14^{\prime}-11^{\prime \prime}$ | 14'-11" | 13'9" | 13'-9" |
|  | 11-7/8" | 19'0" | 19'-0" | 17'-10" | 17'-10" | 16'5" | $16^{\prime}-0$ |
|  | 14 " | 21'7" | 21'7" | 20'3" | 20'-2" | 17'-9" | 16'1" |
|  | $16 "$ | 23-11" | 23-11" | 22'-5" | 20'3" | $17^{\prime}-10^{\prime \prime}$ | $16^{\prime}-2{ }^{\prime \prime}$ |
| $\begin{aligned} & \text { PWI 36L, } \\ & \text { LPI } 36 \end{aligned}$ | 11-7/8" | 19'-10" | 19'-10" | 18'-8" | 18'-8" | 17'-3" | 17'-1" |
|  | 14" | 22'6" | 22'6" | 21'1" | 21'1" | 18'-11" | $17^{\prime}-2$ " |
|  | $16 "$ | 24'10" | $24^{\prime}-10^{\prime \prime}$ | 23'4" | 21'-7" | 19'0" | $17^{\prime}-2{ }^{\prime \prime}$ |
| PWI 42S, LPI 42Plus | 9-1/2" | 18'0" | 18'0" | 16'-11" | 16'11" | 15'-7" | $15^{\prime}-7{ }^{\prime \prime}$ |
|  | 11-7/8" | 21'7" | 21'7" | 20'3" | 20'3" | 18'8" | 18'8" |
|  | $14^{\prime \prime}$ | $24^{\prime}$ '6" | 24'-6" | 23'0" | 23'0" | 21'3" | 21'3" |
|  | $16 "$ | 27'-2" | 27'-2" | 25'-6" | 25'6" | 23'7" | 22'-5" |
| PWI 52S, LPI 52Plus | 11-7/8" | 22'3" | 22'3" | 20'-11" | 20'-11" | 19'4" | 19'-4" |
|  | 14 " | 25'-4" | 25'-4" | 23'-9" | 23'-9" | 22'0" | 22'0" |
|  | $16{ }^{\prime \prime}$ | 28-0" | 28-0" | 26'4" | 26'4" | $24^{\prime}-4 \prime$ | 23'-10" |
| PWI 56L, LPI 56 | 11-7/8" | 23'0" | 23'0" | 21'7" | 21'7" | 20'0" | 19'-3" |
|  | $14^{\prime \prime}$ | 26'-1" | 26'1" | 24'-6" | 24'-2" | 21'3" | 19'-3" |
|  | $16 "$ | 28-10" | 28-10" | 26'-8" | 24'-2" | 21'-3" | 19'-3" |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 50 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" Oc |  | 19.2" oc |  | 24" OC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 12'-8" | 12'-8" | 11'11" | 11'-11" | 11'-0" | 11-0" |
|  | 11-7/8" | 15'-4" | $15^{\prime}-4 "$ | $14^{\prime}-4^{\prime \prime}$ | 13'-11" | $13^{\prime}-0^{\prime \prime}$ | $12^{\prime}-4 "$ |
| PWI 20S, LPI 20Plus | 9-1/2" | 13-10" | 13'10" | 13'0" | 13'0" | 12'-0" | $12^{\prime}-0 "$ |
|  | 11-7/8" | 16'7" | 16'7" | 15'7" | 15'7" | 14'-5" | 13'10" |
|  | $14 "$ | 19'0" | 19'0" | 17'-10" | 17'-5" | 15'1" | 13'-10" |
|  | $16^{\prime \prime}$ | 21'-2" | 21'0" | 19'0" | $17^{\prime}-6{ }^{\prime \prime}$ | 15'-2" | 13-11" |
| PWI 32S, LPI 32Plus | 9-1/2" | $14^{\prime}-8$ " | 14 '8" | 13'-9" | 13'-9" | 12'-9" | 12 '9" |
|  | 11-7/8" | $17^{\prime \prime}-7{ }^{\prime \prime}$ | $17^{\prime}-7{ }^{\prime \prime}$ | 16'-5" | $16^{\prime}-5{ }^{\prime \prime}$ | 15'-0" | 13'10" |
|  | 14 " | 19'-11" | 19'-11" | 18'9" | 17'-5" | 15'1" | 13'-10" |
|  | $16 "$ | 22'-1" | 21'0" | 19'0" | $17^{\prime}-6 "$ | $15^{\prime}-2{ }^{\prime \prime}$ | 13-11" |
| $\begin{gathered} \text { PWI 36L, } \\ \text { LPI } 36 \end{gathered}$ | 11-7/8" | 18'-4" | 18'-4" | 17'-3" | 17'-3" | 15'-11" | 14 '9" |
|  | $14^{\prime \prime}$ | 20'-10" | 20'-10" | 19'-6" | 18'7" | 16'-1" | 14'-9" |
|  | $16 "$ | 23'0" | 22'-5" | 20'3" | 18'7" | 16'-2" | $14^{\prime}-10^{\prime \prime}$ |
| PWI 42S, LPI 42Plus | 9-1/2" | 16'-8" | 16'8" | $15 ' 7{ }^{\prime \prime}$ | 15'-7" | 14'-5" | 14'-5" |
|  | 11-7/8" | 19'-11" | 19'-11" | 18'8" | 18'-8" | 17'-3" | 17'-3" |
|  | $14{ }^{\prime \prime}$ | 22'-8" | 22'-8" | 21'-3" | 21'-3" | 19'-8" | 18'8" |
|  | $16^{\prime \prime}$ | 25'-2" | 25'-2" | 23'-7" | 23'7" | 21'-0" | 19'-4" |
| PWI 52S,LPI 52Plus | 11-7/8" | 20'-8" | 20'-8" | $19^{\prime}-4$ " | 19'-4" | 17'-11" | 17'-11" |
|  | $14{ }^{\prime \prime}$ | 23'-5" | 23'-5" | 22'-0" | 22'-0" | 20'4" ${ }^{\prime \prime}$ | 20'1" |
|  | $16^{\prime \prime}$ | 25-11" | 25'-11" | 24'-4" | 24'-4" | 22'-4" | 20'6" |
| PWI 56L, LPI 56 | 11-7/8" | 21'-4" | 21'-4" | 20'-0" | 20'-0" | 18'0" | 16'7" |
|  | $14^{\prime \prime}$ | 24'-2" | 24'-2" | 22'-8" | 20'-10" | 18'1" | 16'-7" |
|  | $16^{\prime \prime}$ | 26'-8" | 25'-1" | 22'-8" | 20'-10" | 18'-1" | $16^{\prime}-7{ }^{\prime \prime}$ |

SPECIFIED SNOW LOAD (STANDARD DURATION) - 60 PSF SNOW

| Series Depth <br> Specified Dead Load $\rightarrow$  |  | 16" oc |  | 19.2" OC |  | 24"0c |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 15 psf | 20 psf | 15 psf | 20 psf | 15 psf | 20 psf |
| PWI 18S, LPI 18 | 9-1/2" | 11'11" | 11'-11" | $11^{\prime}-2$ " | 11'-2" | $10^{\prime}-4{ }^{\prime \prime}$ | 10'-4" |
|  | 11-7/8" | 14'-4" | 14'-4" | $13^{\prime}-6 "$ | $13^{\prime \prime} \mathbf{1 '}^{\prime \prime}$ | 11'-8" | 10'-10" |
| PWI 20S, LPI 20Plus | 9-1/2" | $13^{\prime}-0$ " | $13^{\prime}-0 "$ | $12^{\prime}-2$ " | $12^{\prime}-2$ " | 11'-3" | 11'-3" |
|  | 11-7/8" | 15'7" | 15'-7" | $14^{\prime}-7{ }^{\prime \prime}$ | $14^{\prime}-7{ }^{\prime \prime}$ | $13^{\prime \prime} \mathbf{1}^{\prime \prime}$ | $12^{\prime \prime} 1^{\prime \prime}$ |
|  | 14 | 17'-10" | 17'-10" | $16^{\prime}$ '6" | 15'-3" | 13 '1" | $12^{\prime}-2$ " |
|  | $16 "$ | 19'10" | 18'6" | 16'6" | $15^{\prime}-4 "$ | $13^{\prime \prime} 2^{\prime \prime}$ | $12^{\prime}-3 "$ |
| $\begin{aligned} & \text { PWI 32S, } \\ & \text { LPI 32Plus } \end{aligned}$ | 9-1/2" | 13'-9" | 13'9" | 12'-11" | 12'-11" | 11'-11" | 11-11" |
|  | 11-7/8" | 16'5" | 16'5" | 15'-5" | 15'-3" | 13'1" | $12^{\prime}-1$ " |
|  | 14 " | 18'9" | 18'-5" | $16^{\prime}-6 "$ | $15^{\prime}-3 "$ | 13'1" | $12^{\prime}-2{ }^{\prime \prime}$ |
|  | $16 "$ | 19'-11" | 18'6" | $16^{\prime}$ '6" | $15^{\prime}-4{ }^{\prime \prime}$ | $13^{\prime \prime} 2^{\prime \prime}$ | 12'-3" |
| PWI 36L, LPI 36 | 11-7/8" | 17'-3" | 17'-3" | $16^{\prime}-2{ }^{\prime \prime}$ | $16^{\prime}-2{ }^{\prime \prime}$ | 13'-11" | 12'-11" |
|  | 14 " | 19'6" | 19'6" | 17'-7" | $16^{\prime} \cdot 3$ " | $14^{\prime}-0{ }^{\prime \prime}$ | $13^{\prime} \cdot 0$ " |
|  | $16 "$ | 21'-2" | 19'-8" | $17^{\prime}-7{ }^{\prime \prime}$ | $16^{\prime}-4$ " | $14^{\prime}-0 "$ | $13^{\prime}-0 "$ |
| PWI 42S, LPI 42Plus | 9-1/2" | 15'7" | 15'-7" | 14'-8" | 14'-8" | 13'6" | 13'6" |
|  | 11-7/8" | 18'8" | 18'8" | $17^{\prime \prime}$ " | 17'-6" | $16^{\prime}-2{ }^{\prime \prime}$ | 15'9" |
|  | 14 " | 21'3" | 21'3" | 20'0" | 20'0" | 17'-8" | 16'-5" |
|  | $16 "$ | 23'7" | 23'7" | 22'-2" | 21'-4" | 18'-3" | $17^{\prime}-0{ }^{\prime \prime}$ |
| PWI 52S, LPI 52Plus | 11-7/8" | 19'-4" | 19'-4" | 18'-2" | 18'-2" | 16'-10" | 16'-10" |
|  | 14 " | 22'0" | 22'0" | 20'-8" | 20'-8" | 19'1" | 17'-8" |
|  | $16 "$ | 24'4" | 24'-4" | 22-10" | 22'-8" | 19'-5" | 18'0" |
| PWI 56L, LPI 56 | 11-7/8" | 20'0" | 20'0" | 18'-9" | 18'-3" | 15'-8" | $14^{\prime}-6{ }^{\prime \prime}$ |
|  | $14^{\prime \prime}$ | 22'-8" | 22'0" ${ }^{\prime \prime}$ | 19'-8" | 18'-3" | $15^{\prime}-8{ }^{\prime \prime}$ | $14^{\prime}-7{ }^{\prime \prime}$ |
|  | $16 "$ | 23'9" | 22'-1" | 19'-9" | 18'-4" | 15'-9" | $14^{\prime}-7{ }^{\prime \prime}$ |

Table Usage:

1. Select the appropriate set of tables based on roof pitch.
2. Select the section of that table that corresponds to the specified roof live or snow load.
3. Find a span that meets or exceeds the design span for the appropriate specified roof dead load ( 15 psf or 20 psf).
4. Read the corresponding series, depth and spacing.

Design Assumptions:

1. The spans listed are the horizontal clear distance between supports and are valid for simple or continuous span applications. Continuous spans are based on the longest span. The shortest span shall not be less than $50 \%$ of the longest span.
2. The spans are based on uniform gravity loads only as listed for each table, including the effects of a 300 lb concentrated load. These spans have not been evaluated for wind.
3. These tables do not reflect any additional stiffness provided by the roof sheathing
4. Live load deflection is limited to $\mathrm{L} / 360$.
5. Total load deflection is limited to $\mathrm{L} / 180$.
6. The spans are based on an end bearing length of at least $1-3 / 4$ " and an interior bearing length of at least $3-1 / 2$," and are limited to the bearing capacity for an SPF wall plate.
7. These tables assume full lateral support of the compression flange. Full support is considered to be a maximum unbraced length of 24 "

## Additional Notes:

1. Web stiffeners are not required for the Roof Span tables except when using a "bird's mouth" detail for the low-end bearing.
2. Web fillers are required for 1 -Joists seated in hangers that do not laterally support the top flange or for hangers that require nailing into the web.
3. $\mathrm{L} / 360$ represents the maximum deflection allowed per code for roof joists supporting plaster or gypsum ceilings. Verify deflection limits with local code requirements.
4. Roof joists must have a minimum pitch of $1 / 4$ " per foot (1/4:12) for positive drainage.
5. Roof applications in high wind areas require special analysis which may reduce spans and may require bracing of the bottom flange and special connectors to resist uplift.
6. For conditions not shown, use the Uniform Roof Load (PLF) tables, use the Exacte by PWT software or contact your PWT ${ }^{\text {mid }}$ distributor for assistance.


ACTUAL DEFLECTION BASED ON SPAN AND LIMIT

| Span (ft) | L/360 | L/240 | L/180 |
| :---: | :---: | :---: | :---: |
| 10' | 5/16" | 1/2" | 11/16" |
| $12 '$ | 3/8" | 5/8" | 13/16" |
| $14^{\prime}$ | 7/16" | 11/16" | 15/16" |
| $16^{\prime}$ | 9/16" | 13/16" | 1-1/16" |
| $18{ }^{\prime}$ | 5/8" | 7/8" | 1-3/16" |
| 20' | 11/16" | 1" | 1-5/16" |
| $22^{\prime}$ | 3/4" | 1-1/8" | 1-7/16" |
| $24^{\prime}$ | 13/16" | 1-3/16" | 1-5/8" |
| $26^{\prime}$ | 7/8" | 1-5/16" | 1-3/4" |
| $28^{\prime}$ | 15/16" | 1-3/8" | 1-7/8" |
| 30' | $1^{\prime \prime}$ | 1-1/2" | $2{ }^{\prime \prime}$ |

[^2]
## Cantilever Details



## Brick-Ledge Cantilevers

TOTAL JOIST REACTION CALCULATION
PWT ${ }^{\text {TM }} 1$-Joists can cantilever up to 6 " to support a load-bearing wall over a brick finish. Depending on the Total Joist Reaction (TJR), the joists may require reinforcement. If the TJR is less than the End Reaction Capacity W/out Stiffeners (page 4), then no reinforcement is required. If the TJR is greater than the End Reaction Capacity W/out Stiffeners, but less than the End Reaction Capacity With Stiffeners, then web stiffeners shall be installed at the bearing. Otherwise, one of the reinforcing details shall be used.

Total Joist Reaction, TJR = FLR + WLR + RLR
Where: FLR = Floor Load Reaction
WLR = Wall Load Reaction
RLR = Roof Load Reaction, including any other floor, ceiling or attic loads imposed on wall


## EXAMPLE 1:I-JOIST: 9-1/2" PWI 205 - WALL UNDER CANTILEVER: 3-1/2" WIDE

| Specified Design Loads: | Floor System: | Roof System: |
| :---: | :---: | :---: |
| Floor: 40/10 psf | Joist Span = 16' | Roof Span = 22' |
| Roof: 20/10 psf | Joist Cantilever $=5^{\prime \prime}$ | Roof Overhang = $1^{\prime}$ |
| Wall: 80 plf | Joist Spacing $=16^{\prime \prime} 00$ |  |
| Factored FLR | $\begin{aligned} & =(\text { Joist Span / } 2+\text { Jois } \\ & \text { (Joist Spacing / 12) } \\ & =\left(16^{\prime} / 2+5^{\prime \prime} / 12\right)^{*} \\ & =814 \mathrm{lbs} \end{aligned}$ | ver / 12) * (Factored <br> psf + 1.25 * 10 psf |

Factored WLR $=\left(\right.$ Factored Wall Load) ${ }^{*}$ (Joist Spacing / 12)
$=\left(1.25^{*} 80 \mathrm{plf}\right){ }^{*}\left(16^{\prime \prime} / 12\right)$
$=133 \mathrm{lbs}$
Factored RLR $=\left(\right.$ Roof Span $/ 2+$ Roof Overhang) ${ }^{*}\left(\right.$ Factored Roof Load) ${ }^{*}$ (Joist Spacing / 12)
$=\left(22^{\prime} / 2+1^{\prime}\right) *\left(1.5^{*} 20 \mathrm{psf}+1.25^{*} 10 \mathrm{psf}\right)^{\star}\left(16^{\prime \prime} / 12\right)$
$=680 \mathrm{lbs}$
Factored TJR $=814+133+680$
$=1627 \mathrm{lbs}$

FACTORED END REACTION RESISTANCE

| 9-1/2" PWI 20S on a 3-1/2" wall | Min. <br> 1-1/2" Bearing | Max. <br> 4" Bearing | 3-1/2" <br> Bearing |
| :--- | :---: | :---: | :---: |
| Without Web Stiffeners | 1530 | 1750 | 1706 |
| With Web Stiffeners | 1800 | 1990 | 1952 |
| With Web Filler Reinforcing | - | - | 3660 |
| With 23/32 APA Rated OSB <br> Full-Depth Reinforcing (One Side) | - | - | 4930 |
| With 1" OSB Rim Full-Depth <br> Reinforcing (One Side) | - | - | 5350 |

Since the Factored Total Joist Reaction, 1627 lbs ., is less than the Factored End Reaction Resistance w/out Stiffeners for 3-1/2" bearing ( 1706 lbs .), no reinforcement is required.

## EXAMPLE 1:I-JOIST: 11-7/8" PWI 32S - WALL UNDER CANTILEVER: 3-1/2" WIDE

| Specified Design Loads: <br> Floor: 40/15 psf <br> Roof: 30/15 psf <br> Wall: 100 plf | Floor System: Roof System: <br> Joist Span $=16^{\prime}$ Roof Span = 32' <br> Joist Cantilever $=5^{\prime \prime}$ Roof Overhang = 1' <br> Joist Spacing $=24^{\prime \prime}$ oc  |
| :---: | :---: |
| Factored FLR | $\begin{aligned} & =\left(\begin{array}{l} \left.(\text { Joist Span } / 2+\text { Joist Cantilever } / 12)^{*} \text { (Factored Floor Load) }\right)^{\prime} \\ (\text { Joist Spacing / 12) } \\ =\left(16^{\prime} / 2+5^{\prime \prime} / 12\right)^{*}\left(1.5^{*} 40 \text { psf }+1.5^{*} 15 \text { psf }\right)^{*}\left(24^{\prime \prime} / 12\right) \\ =1326 \text { lbs } \end{array}\right. \end{aligned}$ |
| Factored WLR | $\begin{aligned} & =\left(\text { (Factored Wall Load) }{ }^{*}\right. \text { (Joist Spacing / 12) } \\ & =\left(1.25^{\star} 100 \mathrm{plf}\right)^{*}\left(24^{"} / 12\right) \\ & =250 \mathrm{lbs} \end{aligned}$ |
| Factored RL | $\begin{aligned} & \left.=(\text { Roof Span } / 2+\text { Roof Overhang })^{*} \text { (Factored Roof Load) }\right)^{*} \\ & (\text { Joist Spacing } / 12) \\ & =\left(32^{\prime} / 2+1^{\prime}\right)^{*}\left(1.5 * 30 \text { psf }+1.25^{*} 15 \text { psf) }\right)^{*}\left(24^{\prime \prime} / 12\right) \\ & =2168 \mathrm{lds} \end{aligned}$ |
| Factored TJR | $\begin{aligned} & =1326+250+2168 \\ & =3744 \mathrm{lbs} \end{aligned}$ |

FACTORED END REACTION RESISTANCE

| 11-7/8" PWI 32S on a 3-1/2" wall | Min. <br> 1-1/2" Bearing | Max. <br> 4" Bearing | $3-1 / \mathbf{2 " ~}^{\prime \prime}$ <br> Bearing |
| :--- | :---: | :---: | :---: |
| Without Web Stiffeners | 1530 | 1830 | 1770 |
| With Web Stiffeners | 2010 | 2345 | 2278 |
| With Web Filler Reinforcing | - | - | 3660 |
| With 23/32 APA Rated OSB <br> Full-Depth Reinforcing (One Side) | - | - | 4930 |
| With 1" OSB Rim Full-Depth <br> Reinforcing (One Side) | - | - | 5350 |

Since the Factored Total Joist Reaction, 3744 lbs ., is greater than the Factored End Reaction Resistance with Web Filler Reinforcing ( 3660 lbs .), but is less than the Factored End Reaction Resistance with 23/32 APA Rated OSB Full-Depth Reinforcing ( 4930 lbs .), this joist requires the installation of full-depth reinforcing consisting of a minimum 23/32 APA Rated OSB (or equal) attached to one side (Detail C8) at the bearing.

## Web Hole Specifications Circular Holes



## Table Usage:

1. Select the required series and depth.
2. Determine the support condition for the nearest bearing: end support or interior support (including cantilever-end supports).
3. Select the row corresponding to the required Clear Span. For spans between those listed, use the next largest value.

4 Select the column corresponding to the required hole diameter. For diameters between those listed, use the next largest value.
5. The intersection of the Clear Span row and Hole Diameter column gives the minimum distance from the inside face of bearing to the center of a circular hole.
6. Double check the distance to the other support, using the appropriate support condition.

| Series | Depth | $\begin{aligned} & \text { Clear } \\ & \text { Span } \\ & \text { (ft) } \end{aligned}$ | Distance from End Support |  |  |  |  |  | Distance from Interior or Cantilever-End Support |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Hole Diameter |  |  |  |  |  | Hole Diameter |  |  |  |  |  |
|  |  |  | 2" | 4" | 6 " | 8" | 10" | 12" | 2" | 4" | $6{ }^{\prime \prime}$ | 8" | $10^{\prime \prime}$ | 12" |
| PWI 18S LPI 18 | 9-1/2" | 6 | $1^{\prime}-0^{\prime \prime}$ | 1'0" | 1'-0" | - | - | - | $1^{\prime}-0 /$ | 1'-0" | $1^{\prime}-0^{\prime \prime}$ | - | - | - |
|  |  | 10 | 1'-0" | 1'0" | 2'-1" |  | - | - | 1'0" | 1'-3" | 3'-1" | - | - | - |
|  |  | 14 | 1'-0" | 2'-2" | 4'-6" |  |  | - | 1'-11" | 3'-9" | 5'-7" | - | - | - |
|  |  | 18 | 2'-4" | 4'-7" | 7'-2" |  |  | - | 4'-5" | 6'-3" | 8'-4" | - | - | - |
|  | 11-7/8" | 10 | 1'-0" | 1'0" | 1'-0" | $1^{\prime}-10^{\prime \prime}$ |  | - | 1'-0" | 1'-0" | $1^{\prime}-3$ " | 3'0" | - | - |
|  |  | 14 | 1'-0" | 1'-0" | 2'1" | $4^{\prime}-4{ }^{\prime \prime}$ | - | - | 1'0" | 2'0" | 3'-9" | 5'-6" | - | - |
|  |  | 18 | 1'-0" | 2'-5" | 4'6" | 6'-11" | - | - | 2'-9" | $4^{\prime}-6 "$ | 6'-3" | 8'-1" | - | - |
|  |  | 22 | 2'-8" | 4'-9" | 7'-0" | 9'-8" | - | - | 5'3" | 7'-0" | 8'-9" | $11^{\prime}-0^{\prime \prime}$ | - | - |
| PWI 20S <br> LPI 20Plus <br>  <br> PWI 32S <br> LPI 32Plus | 9-1/2" | 6 | 1'-0" | 1'0" | 1'-0" |  |  |  | 1'0" | 1'0" | 1'0" |  | - | - |
|  |  | 10 | 1'-0" | 1'0" | 1'0" |  |  | - | 1'0" | 1'0" | 1'0" |  | - | - |
|  |  | 14 | 1'-0" | 1'0" | 1'-5" | - | - | - | 1'-0" | 1'-5" | 3'-1" | - | - | - |
|  |  | 18 | 1'-0" | 1'-9" | $3^{\prime}-8{ }^{\prime \prime}$ |  | - | - | 2'-3" | 3'-11" | 5'-7" | - | - | - |
|  | 11-7/8" | 10 | 1'-0" | 1'0" | $1^{\prime}-0^{\prime \prime}$ | 1'0" | - | - | 1'0" | $1^{1}-0{ }^{\prime \prime}$ | 1'-0" | 1'0" | - | - |
|  |  | 14 | 1'-0" | 1'-0" | 1'0" | 1'-9" |  |  | 1'0" | 1'0" | 2'-1" | 3'-5" | - | - |
|  |  | 18 | 1'-0" | 1'-0" | 2'-6" | 4'-1' | - | - | 1'-10" | 3'-3" | 4'-7" | 5'-11" | - | - |
|  |  | 22 | 1'-8" | 3'-2" | 4'-10" | 6'7" |  |  | 4'-4" | 5'9" | 7'1" ${ }^{\prime \prime}$ | 8'-5" |  | - |
|  | 14" | 14 | 1'-0" | 1'0" | 1'-0" | 1'-0" | 2'-2" | - | 1'-0" | 1'-0" | 1'-5" | 2'-7" | 3'-9" | - |
|  |  | 18 | 1'-0" | 1'-0" | 1'-9" | 3'-1" | 4'-6" | - | 1'-8" | 2'-10" | 3'-11' | 5'-1" | 6'-3" | - |
|  |  | 22 | 1'-5" | 2'-9" | 4'-1" | 5'-6" | 7'-0" | - | 4'-2" | 5'-4" | 6'-5" | 7'-7" | 8'-9" | - |
|  |  | 26 | 3'-8" | 5'0" | $6^{\prime}-5$ " | 8'0" | 9'-8" | - | 6'8" | 7'-10" | 8'-11' | 10'-1" | 11'-4" |  |
|  | 16" | 18 | 1'-0" | 1'0" | $1^{\prime \prime}-4{ }^{\prime \prime}$ | 2'-5" | 3'-7" | 4'-11" | 1'-6" | 2'-6" | 3'-6" | 4'-6" | 5'-6" | $6^{\prime}-6{ }^{\prime \prime}$ |
|  |  | 22 | 1'-4" | 2'-5" | $3^{\prime}-6{ }^{\prime \prime}$ | 4'-9" | 6'-1" | 7'-5" | 4'0" | 5'0" | $6^{\prime}-0$ | 7'0" | 8'-0" | 9'-0" |
|  |  | 26 | $3^{\prime \prime} 6^{\prime \prime}$ | 4'-8" | 5'-11" | 7'-2" | 8'-7" | 10'1'1' | 6'-6" | 7'-6" | 8'-6" | 9'-6" | 10'6" | 11'-9" |
|  |  | 30 | 5'-9" | 7'0" | 8'-4" | 9'-9" | $11^{\prime}-3^{\prime \prime}$ | $12^{\prime}-10^{\prime \prime}$ | 9'0" | $10^{\prime}-0^{\prime \prime}$ | 11'0" | 12'-0" | $13^{\prime}-2^{\prime \prime}$ | $14^{\prime}-8^{\prime \prime}$ |
| $\begin{gathered} \text { PWI 36L } \\ \text { LPI } 36 \\ \& \\ \text { PWI } 56 \mathrm{~L} \\ \text { LPI } 56 \end{gathered}$ | 11-7/8" | 10 | 1'-0" | 1'0" | 1'-0" | 1'-0" |  | - | 1'0" | 1'-0" | 1'-0" | 1'-3" |  | - |
|  |  | 14 | 1'-0" | 1'-0" | 1'0" | 2'-2' |  | - | 1'0" | 1'0" | 1'-8" | 3'9" | - | - |
|  |  | 18 | 1'-0" | 1'0" | 2'-0" | 4'-7" |  | - | 1'-0" | 2'-1" | $4^{\prime}-2{ }^{\prime \prime}$ | 6'3" | - | - |
|  |  | 22 | 1'-0" | 1'-11' | $4^{\prime}-4{ }^{\prime \prime}$ | 7'-1" |  | - | 2'-6" | 4'-7" | $6^{\prime}-8{ }^{\prime \prime}$ | 8'-9" | - | - |
|  | 14" | 14 | 1'-0" | 1'-0" | 1'-0" | 1'-0" | $2^{\prime}-10^{\prime \prime}$ | - | 1'-0" | 1'-0" | 1'-0" | 2'-6" | $4^{\prime}-4^{\prime \prime}$ | - |
|  |  | 18 | 1'-0" | 1'-0" | 1'0" | 3'0" ${ }^{\prime \prime}$ | 5'-3" | - | 1'0" | 1'-5" | $3^{\prime}-3^{\prime \prime}$ | 5'0" | $6^{\prime}-10^{\prime \prime}$ | - |
|  |  | 22 | 1'-0" | 1'-3" | $3^{\prime}-2^{\prime \prime}$ | 5'-4" | $7^{\prime \prime}-10^{\prime \prime}$ | - | 2'-2" | 3'-11" | 5'-9" | 7'-6" | 9'-4" | - |
|  |  | 26 | 1'-5" | 3'-5" | 5'-6" | 7'-10" | $10^{\prime}-6{ }^{\prime \prime}$ |  | 4'-8" | 6'-5" | 8'-3" | $10^{\prime}-0^{\prime \prime}$ | $12^{\prime}-2{ }^{\prime \prime}$ | - |
|  | 16" | 18 | 1'-0" | 1'0" | 1'0" | 2'0" | 3'-10" | 5'-11" | 1'0" | 1'-0" | 2'-7" | 4'-1" | 5'-8" | 7'-3" |
|  |  | 22 | 1'-0" | 1'-0" | $2^{\prime}-5 "$ | 4'-3" | 6'-3" | 8'-6" | 1'-11" | 3'-6" | 5'1" | 6'-7" | 8'-2" | 9'-11" |
|  |  | 26 | 1'-3" | 2'-11" | 4'-8" | 6'-8" | 8'-10" | 11'-3" | 4'-5" | 6'0" | 7'-7" | 9'-1" | 10'-8" | 12'-10" |
|  |  | 30 | $3^{\prime \prime}-4{ }^{\prime \prime}$ | 5'-2" | 7'-1" | 9'-2" | 11'5" | $14^{\prime}-0^{\prime \prime}$ | 6'11" | 8'-6" | 10'1" | 11-7" | 13'-5" |  |
| PWI 42S LPI 42Plus | 9-1/2" | 6 | 1'-0" | 1'0" | 1'-0" | - | - | - | 1'0" | 1'-0" | 1'0" | - | - | - |
|  |  | 10 | 1'-0" | 1'-0" | 1'0" | - | - | - | 1'0" | 1'0" | 1'0" | - | - | - |
|  |  | 14 | 1'-0" | 1'0" | 1'-5" | - | - | - | 1'-0" | 1'-5" | 3'-1" | - | - | - |
|  |  | 18 | 1'-0" | 1'-9" | $3^{\prime}-8^{\prime \prime}$ |  |  |  | 2'-3" | 3'-11" | 5'-7" |  |  | - |
| $\begin{gathered} \text { PWI 42S } \\ \text { LPI 42Plus } \\ \& \& \\ \text { PWI 52S } \\ \text { LPI 52Plus } \end{gathered}$ | 11-7/8" | 10 | 1'-0" | 1'0" | $1^{\prime}-0 \mid$ | 1'-0" |  | - | 1'-0" | 1'-0" | 1'-0" | 1'-0" | - | - |
|  |  | 14 | 1'0" | 1'0" | 1'0" | 1'-9" | - | - | 1'0" | 1'0" | 2'-1" | 3'-5" | - | - |
|  |  | 18 | 1'-0" | 1'0" | 2'6" | 4'-1' | - | - | 1'-10" | 3'-3" | 4'-7" | 5'-11" | - | - |
|  |  | 22 | 1'-8" | 3'-2" | 4'-10" | 6'.7" |  |  | 4'-4" | 5'9" | 7'-1" | 8'-5" | - | - |
|  | 14 " | 14 | 1'0" ${ }^{\prime \prime}$ | 1'-0" | 1'-0" | 1'0" ${ }^{\prime \prime}$ | 2'-2" | - | 1'-0" | 1'-0" | 1'-5" | 2'-7" | $3^{\prime}-9{ }^{\prime \prime}$ | - |
|  |  | 18 | $1^{\prime}-0^{\prime \prime}$ | 1'-0" | 1'-9" | 3'-1" | 4'-6" | - | 1'-8" | 2'-10" | 3'-11' | 5'-1" | 6'-3" | - |
|  |  | 22 | 1'-5" | 2'-9" | 4'1" | 5'-6" | 7'-0" | - | 4'-2" | 5'-4" | 6'-5" | 7'-7" | 8'-9" | - |
|  |  | 26 | 3'-8" | 5'0" | $6^{\prime}-5{ }^{\prime \prime}$ | 8'0'0' | 9'-8" | - | 6'-8" | 7'-10" | 8'-11" | 10'-1" | 11'-4" | - |
|  | $16 "$ | 18 | 1'0'0" | 1'-0" | 1'-4" | 2'5" | 3'-7" | 4'-11" | 1'-6" | 2'6" | 3'-6" | 4'-6" | 5'6" | $6^{\prime}-6^{\prime \prime}$ |
|  |  | 22 | 1'-4" | 2'-5" | 3'6" | 4'-9" | 6'-1" | 7'-5" | 4'0" | 5'0" | 6'0" | 7'0" | 8'-0" | $9^{\prime}-0^{\prime \prime}$ |
|  |  | 26 | $3^{\prime}-6{ }^{\prime \prime}$ | 4'-8" | 5'-11" | 7'-2" | 8'-7" | $10^{\prime}-1{ }^{\prime \prime}$ | 6'-6" | 7'-6" | 8'-6" | 9'-6" | $10^{\prime}-6{ }^{\prime \prime}$ | 11'-9" |
|  |  | 30 | 5'-9" | 7'0" | 8'-4" | 9'-9" | 11'-3" | $12^{\prime}-10^{\prime \prime}$ | 9'0'0' | $10^{\prime}-0^{\prime \prime}$ | 11'0" | 12'-0" | 13'-2' | $14^{\prime}-8^{\prime \prime}$ |

Design Assumptions:

1. The hole locations are valid for floor joists supporting only uniform loads. The total uniform load shall not exceed 130 plf (e.g., 40 psf Live Load and 25 psf Dead Load spaced $24^{\prime \prime} 0 c$ ).
2. Hole location is measured from the inside face of bearing to the center of a circular hole, from the closest support.
3. Clear Span has not been verified for these joists and is shown for informational purposes only! Verify that the joist selected will work for the span and loading conditions needed before checking hole location.
4. The maximum hole depth for circular holes is the I-Joist Depth less 4," except the maximum hole depth is 6 " for $9-1 / 2^{" ~ P W I ~ j o i s t s, ~ a n d ~} 8$ " for 11-7/8" PWI joists.
5. Holes cannot be located in the span where designated "-", without further analysis by a design professional.

## Notes:

1. Holes may be placed anywhere within the depth of the joist. A minimum $1 / 4^{\prime \prime}$ clear distance is recommended between the hole and the flanges.
2. Round holes up to $1-1 / 2^{\prime \prime}$ diameter may be placed anywhere in the web.
3. Perforated "knockouts" may be neglected when locating web holes.
4. Holes larger than $1-1 / 2^{\prime \prime}$ are not permitted in cantilevers without special engineering.
5. Multiple holes shall have a clear separation along the length of the joist of at least twice the larger dimension of the larger adjacent hole, or a minimum of 12" center-to-center, whichever is greater.
6. Multiple holes may be spaced closer provided they fit within the boundary of an acceptable larger hole. Example: two 3" round holes aligned parallel to the joist length may be spaced 2" apart (clear distance) provided that a $3 "$ high by $8^{\prime \prime}$ long rectangle or an $8 "$ diameter round hole are acceptable for the joist depth at that location and completely encompass the holes.
7. For conditions not covered in this table, use the Exacte by PWT software or contact your PWT ${ }^{\text {TM }}$ distributor for assistance.

## Web Hole Specifications Rectangular Holes



## Table Usage:

1. Select the required series and depth.
2. Determine the support condition for the nearest bearing: end support or interior support (including cantilever-end supports).
3. Select the row corresponding to the required Clear Span. For spans between those listed, use the next largest value.

4 Select the column corresponding to the required hole dimension (width or depth). For dimensions between those listed, use the next largest value.
5. The intersection of the Clear Span row and Hole Dimension column gives the minimum distance from the inside face of bearing to the nearest edge of a square or rectangular hole.
6. Double check the distance to the other support, using the appropriate support condition.

| Series | Depth | $\begin{aligned} & \text { Clear } \\ & \text { Span } \\ & \text { (ft) } \end{aligned}$ | Distance from End Support |  |  |  |  |  | Distance from Interior or Cantilever-End Support |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Maximum Hole Dimension: Depth or Width |  |  |  |  |  | Maximum Hole Dimension: Depth or Width |  |  |  |  |  |
|  |  |  | 2" | $4^{\prime \prime}$ | 6" | 8" | 10" | 12" | 2" | 4 " | $6{ }^{\prime \prime}$ | 8" | $10^{\prime \prime}$ | 12" |
| PWI 18S LPI 18 | $91 / 2$ " | 6 | 1'0" | 1'0" | 1'0" | $1^{\prime}-0^{\prime \prime}$ | $1^{\prime}-2^{\prime \prime}$ | 1'-7" | 1'0" | $1^{\prime}-0^{\prime \prime}$ | 1'-3" | 1'-6" | 1'-10" | $2^{\prime}-2{ }^{\prime \prime}$ |
|  |  | 10 | 1'0" | 1'4" | 2'-10" | $3^{\prime}-3^{\prime \prime}$ | 3'-9" | 4'-3" | 1'3" | 2'6" | 3'-9" | 4'-0" | 4'-5" | - |
|  |  | 14 | 2'2" | 3'8" | 5'-5" | 5'-11" | $6^{\prime}-6 "$ | - | 3'-9" | 5'0" | 6'-4" | - | - | - |
|  |  | 18 | $4^{\prime} 7{ }^{\prime \prime}$ | 6'-3" | 8'-2" |  |  | - | $6^{\prime}-3$ " | 7'-6" |  |  | - | - |
|  | 11\%" | 10 | 1'0" | 1'-0" | 2'-2" | $3^{\prime}-6{ }^{\prime \prime}$ | $4^{\prime}-01$ | - | 1'-1" | 2'-2" | $3^{\prime}-2^{\prime \prime}$ | $4^{\prime}-2^{\prime \prime}$ | - | - |
|  |  | 14 | 2'0" | 3'-3" | 4'8" ${ }^{\text {" }}$ | $6^{\prime}-3$ " |  |  | 3'7" | 4'-8" | 5'-8" | - | - |  |
|  |  | 18 | 4'-4" | 5'-9" | 7'3" |  | - |  | $6^{\prime}-1{ }^{\prime \prime}$ | 7'-2" | 8'-5" | - | - | - |
|  |  | 22 | $6^{\prime}-10^{\prime \prime}$ | 8'-4" | 10'-1" |  |  |  | 8'7" | 9'-9" |  | - | - | - |
| $\begin{gathered} \text { PWI 20S } \\ \text { LPI 20Plus } \\ \& \\ \text { PWI 32S } \\ \text { LPI 32Plus } \end{gathered}$ | 9112" | 6 | 1'0" | 1'-0" | 1'-0" | 1'-0" | 1'-0" | 1'-5" | 1'0" | 1'-0" | 1'-0" | 1'-3" | 1'-8" | $2^{\prime}-0^{\prime \prime}$ |
|  |  | 10 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | 2'6" | 2'-11" | 3'-5" | 3'-11" | 1'0" | 2'-1" | 3'-5" | 3'-9" | $4^{\prime}-2^{\prime \prime}$ | - |
|  |  | 14 | 1'7" | 3'-2" | 5'0" | 5'-7" | 6'-1" |  | 3'3" | 4'-7" | 5'-11" | 6'5" | - | - |
|  |  | 18 | 3'-11" | 5'-8" | 7'-9" | 8'-4" |  |  | 5'-9" | 7'-1" |  |  |  |  |
|  | 117\%" | 10 | 1'-0" | 1'-0" | 1'-9" | 3'-3" | $3^{\prime}-9{ }^{\prime \prime}$ | $4^{\prime}-3$ " | 1'-0" | 1'-9" | $2^{\prime}-10^{\prime \prime}$ | $4^{\prime}-0{ }^{\prime \prime}$ | 4'-5" | - |
|  |  | 14 | $1^{\prime}$ '5" ${ }^{\prime \prime}$ | 2'-9" | $4^{\prime}-2{ }^{\prime \prime}$ | $5^{\prime}-11^{\prime \prime}$ | 6'-6" |  | 3'-1" ${ }^{\prime \prime}$ | 4'-3" | 5'-4" | - | - | - |
|  |  | 18 | 3'-8" | 5'-2" | 6'-9" | 8'-8" | - |  | 5'-7" | 6'-9" | 7'-11' | - | - | - |
|  |  | 22 | 6'-1' | 7'-9" | 9'-6" |  |  |  | 8'1" | 9'-3" |  |  | - | - |
|  | 14" | 14 | 1'0" | 1'-0" | 1'-0" | 2'-8" | 4'-11" | 5'-9" | 1'-0" | 1'-0" | 2'-6" | $4^{\prime}-2^{\prime \prime}$ | 5'-10" | - |
|  |  | 18 | 1'0" | 1'-0" | 2'-11" | 5'-1" | $7^{\prime}-7^{\prime \prime}$ | 8'-6" | 1'-7" | 3'-3" | 5'0" | 6'-8" |  | - |
|  |  | 22 | 1'-4" | 3'-3" | 5'-4" | 7'-8" | 10'5" |  | 4'-1" | 5'-9" | 7'-6" | 9'-2" |  | - |
|  |  | 26 | $3^{\prime \prime} 6^{\prime \prime}$ | 5'-7" | 7'-10" | $10^{\prime}-4{ }^{\prime \prime}$ |  |  | 6'-7" | 8'-3" | 10'-0" | 12'-0" | - | - |
|  | 16" | 18 | $1^{\prime}-0^{\prime \prime}$ | 1'-0" | 2'-5" | 4'-4" | 6'-5" |  | 1'-5" | 3'0" | 4'-6" | 6'-1" | 7'-8" | - |
|  |  | 22 | 1'-2" | 2'-11" | 4'-9" | $6^{\prime}-10^{\prime \prime}$ | $9^{\prime}-2^{\prime \prime}$ |  | 3'-11" | 5'6" | 7'0" | 8'-7" | $10^{\prime}-6{ }^{\prime \prime}$ | - |
|  |  | 26 | $3^{\prime}-4^{\prime \prime}$ | 5'-2" | 7'-2" | $9^{\prime} \cdot 5 "$ | 11'-11" |  | 6'-5" | 8'-0" | 9'-6" | 11'-1' |  | - |
|  |  | 30 | $5^{\prime}-8{ }^{\prime \prime}$ | 7'-7" | 9'-9" | 12'-1" |  |  | 8'-11" | 10'6" | 12'-0' | $14^{\prime}-0^{\prime \prime}$ | - | - |
| $\begin{gathered} \text { PWI 36L } \\ \text { LPI } 36 \\ \& \\ \text { PWI } 56 \mathrm{~L} \\ \text { LPI } 56 \end{gathered}$ | 11\%" | 10 | $1^{\prime}-0^{\prime \prime}$ | 1'-0" | $1^{\prime \prime}-9{ }^{\prime \prime}$ | 3'-3" | 3'-9" | 4'-3" | 1'-0" | 1'-9" | 2'-10" | 4'-0" | $4^{\prime}-5^{\prime \prime}$ | - |
|  |  | 14 | 1'-5" | 2'-9" | $4^{\prime}-2^{\prime \prime}$ | 5'-11" | 6'6" |  | 3'-1" | 4'-3" | 5'-4" |  |  | - |
|  |  | 18 | $3^{\prime}-8^{\prime \prime}$ | 5'-2" | 6'-9" | 8'-8" |  |  | 5'-7" | 6'-9" | $7^{\prime}-11^{\prime \prime}$ | - | - | - |
|  |  | 22 | 6'-1" | 7'-9" | 9'-6" |  |  |  | 8'-1"' | 9'-3" |  | - | - | - |
|  | 14" | 14 | 1'0" | 1'-0" | 1'-0" | $2^{\prime}-8{ }^{\prime \prime}$ | 4'-11" | 5'-9" | 1'-0" | 1'-0" | $2^{\prime}-6 "$ | 4'-2' | 5'-10" | - |
|  |  | 18 | 1'0" $0^{\prime \prime}$ | 1'-0" | 2'-11" | 5'-1" | $7^{\prime}-7^{\prime \prime}$ | 8'6" | $1^{\prime}-7{ }^{\prime \prime}$ | 3'-3" | 5'0" | 6'-8" | - | - |
|  |  | 22 | 1'-4" | 3'-3" | 5'-4" | $7^{\prime}-8{ }^{\prime \prime}$ | 10'5" |  | $4^{\prime}-1{ }^{\prime \prime}$ | 5'-9" | 7'-6" | $9^{\prime}-2^{\prime \prime}$ | - | - |
|  |  | 26 | $3^{\prime}-6{ }^{\prime \prime}$ | 5'-7" | 7'-10" | $10^{\prime}-4{ }^{\prime \prime}$ |  |  | $6^{\prime} \cdot 7{ }^{\prime \prime}$ | 8'-3" | 10'0" | 12'0'01 | - |  |
|  | 16 " | 18 | 1'0" | 1'-0" | 2'5" | 4'-4" | 6'5" |  | 1'-5" | 3'-0" | 4'-6" | 6'-1" | 7'-8" | - |
|  |  | 22 | 1'2" | 2'-11" | 4'9" | $6^{\prime}-10^{\prime \prime}$ | 9'2" | - | 3'-11" | 5'-6" | 7'0" | 8'-7" | $10^{\prime}-6{ }^{\prime \prime}$ | - |
|  |  | 26 | 3'4" | 5'-2" | 7'-2" | 9'-5" | 11'-11" | - | 6'-5" | 8'0" | 9'-6" | 11'1'1' | - | - |
|  |  | 30 | 5'8" | 7'-7" | 9'-9" | 12'-1" |  | - | 8'-11' | 10'6" | 12'0" | $14^{\prime}-0^{\prime \prime}$ | - | - |
| PWI 42SLPI 42Plus | 911/2 | 6 | 1'0" | 1'-0" | 1'0" | 1'-0" | $1^{\prime}-0^{\prime \prime}$ | 1'-5" | 1'0" | 1'-0" | 1'-0" | 1'-3" | 1'-8" | $2^{\prime \prime} 0^{\prime \prime}$ |
|  |  | 10 | 1'0" | 1'-0" | 2'6" | 2'-11' | 3'-5" | 3'-11" | 1'-0" | 2'-1" | 3'-5" | 3'-9" | 4'-2" | - |
|  |  | 14 | 1'-7" | 3'-2' | 5'0" | 5'-7" | 6'-1" |  | 3'3" | 4'-7" | 5'-11" | 6'5" | - | - |
|  |  | 18 | 3'-11' | 5'-8" | 7'9" | 8'-4" |  | - | 5'-9" | 7'-1" |  | - | - | - |
| $\begin{gathered} \text { PWI 42S } \\ \text { LPI 42Plus } \\ \& \& \\ \text { PWI 52S } \\ \text { LPI 52Plus } \end{gathered}$ | 11/8" | 10 | 1'-0" | 1'0" | 1'9" | 3'-3" | 3'-9" | 4'-3" |  | 1'-9" | $2^{\prime}-10^{\prime \prime}$ | $4^{\prime}-0^{\prime \prime}$ | 4'-5" | - |
|  |  | 14 | $1^{\prime} 5^{\prime \prime}$ | 2'9" | $4^{\prime}-2{ }^{\prime \prime}$ | 5'-11" | 6'6" |  | 3'-1" ${ }^{\prime \prime}$ | 4'-3" | $5^{\prime}-4{ }^{\prime \prime}$ | - | - | - |
|  |  | 18 | 3'-8" | 5'-2" | 6'9" | 8'-8" | - | - | 5'-7" | 6'-9" | 7'-11' | - | - | - |
|  |  | 22 | 6'1'1' | 7'-9" | 9'6" | - | - | - | 8'-1" | 9'-3" | - | - | - | - |
|  | 14 " | 14 | 1'-0" | 1'0" ${ }^{\prime \prime}$ |  | 2'-8" | 4'-11" ${ }^{\prime \prime}$ | 5'-9" | 1'-0" | 1'-0" | 2'-6" | $4^{\prime}-2^{\prime \prime}$ | $5^{\prime}-10^{\prime \prime}$ | - |
|  |  | 18 | $1^{1}-0^{\prime \prime}$ | 1'0" | 2'-11" | 5'-1" | 7'-7" | 8'-6" | 1'-7" | 3'3" ${ }^{\prime \prime}$ | 5'0" ${ }^{\prime \prime}$ | 6'-8" |  | - |
|  |  | 22 | 1'-4" | $3^{\prime}-3^{\prime \prime}$ | 5'-4" | $7^{1}-8{ }^{\prime \prime}$ | $10^{\prime}-5 "$ |  | 4'-1" | 5'-9" | $7^{\prime}-6{ }^{\prime \prime}$ | $9^{\prime}-2^{\prime \prime}$ | - | - |
|  |  | 26 | 3'-6" | 5'-7" | 7'-10" | $10^{\prime}-4{ }^{\prime \prime}$ | - |  | 6'-7" | 8'-3" | 10'0" | 12'-0" | - | - |
|  | $16 "$ | 18 | $1^{\prime}-0^{\prime \prime}$ | 1'-0" | 2'5" | 4'-4" | 6'5" |  | 1'-5" | 3'0" | 4'-6" | 6'-1" | 7'-8" | - |
|  |  | 22 | 1'-2" | 2'-11" | 4'-9" | 6'-10" | $9^{\prime}-2^{\prime \prime}$ |  | 3'-11" | 5'6" | 7'0" | 8'-7" | $10^{\prime}-6{ }^{\prime \prime}$ | - |
|  |  | 26 | $3^{\prime}-4{ }^{\prime \prime}$ | 5'2" ${ }^{\prime \prime}$ | 7'-2" | $9^{\prime}$ '5" ${ }^{\prime \prime}$ | 11'-11" |  | 6'5" | 8'0'0' | $9^{\prime} \mathbf{' V}^{\prime \prime}$ | 11'-1" | - | - |
|  |  | 30 | 5'-8" | 7'-7" | 9'-9" | $12^{\prime}-1{ }^{\prime \prime}$ |  | - | 8'-11" | $10^{\prime}-6{ }^{\prime \prime}$ | 12'-0" | $14^{\prime}-0^{\prime \prime}$ | - | - |

## Design Assumptions:

1. The hole locations are valid for floor joists supporting only uniform loads. The total uniform load shall not exceed 130 plf (e.g., 40 psf Live Load and 25 psf Dead Load spaced 24" oc).
2. Hole location is measured from the inside face of bearing to the nearest edge of a rectangular hole, from the closest support.
3. Clear Span has not been verified for these joists and is shown for informational purposes only! Verify that the joist selected will work for the span and loading conditions needed before checking hole location.
4. The maximum hole depth for rectangular holes is the I-Joist Depth less 4," except the maximum hole depth is 6 " for $9-1 / 2^{\prime \prime}$ PWI joists, and $8^{\prime \prime}$ for $11-7 / 8^{\prime \prime}$ PWI Joists. Where the Maximum Hole Dimension exceeds the hole depth, the dimension refers to hole width and the depth of the hole is assumed to be the maximum for that joist depth. The maximum hole width is 18," regardless of I-Joist Depth.
5. Holes cannot be located in the span where designated "-", without further analysis by a design professional.

## Notes:

1. Holes may be placed anywhere within the depth of the joist. A minimum $1 / 4^{\prime \prime}$ clear distance is recommended between the hole and the flanges.
2. Round holes up to $1-1 / 2^{\prime \prime}$ diameter may be placed anywhere in the web.
3. Perforated "knockouts" may be neglected when locating web holes.
4. Holes larger than $1-1 / 2^{\prime \prime}$ are not permitted in cantilevers without special engineering.
5. Multiple holes shall have a clear separation along the length of the joist of at least twice the larger dimension of the larger adjacent hole, or a minimum of 12" center-to-center, whichever is greater.
6. Multiple holes may be spaced closer provided they fit within the boundary of an acceptable larger hole. Example: two 3" round holes aligned parallel to the joist length may be spaced 2" apart (clear distance) provided that a 3 " high by $8^{" 1}$ long rectangle or an 8 " diameter round hole are acceptable for the joist depth at that location and completely encompass the holes.
7. For conditions not covered in this table, use the Exacte by PWT software or contact your PWT ${ }^{\text {mw }}$ distributor for assistance.

## Floor Details

|  |  | (A3) Blocking at exterior wall <br> OSB or PWT LVL Rim may be substituted for PWI blocking |
| :---: | :---: | :---: |
| (A4) SOLID BLOCKING AT EXTERIOR WALL | (A5) JOIST SUPPORT NAILING <br> Place nail 1-1/2" min from end of 1 -Joist. If nails are close to edge of plate, drive at an angle to reduce splititing | B1 WEB STIFFENERS AT INTERIOR SUPPORT (when neuuneo) <br> Verify stiffener requirements (see Web Stiffener detail) |
|  |  | NON-STACKING WALLS <br> PWT I-Joists shall be designed to carry all applied loads including walls from above that do not stack directly over the 1 -Joist support. |
| (D2) POST LOADS | (E1) stalr stringer <br> See I-Joist Header CrossSection for connection <br> See I-Joist Filler and backer blocks Schedule for filler block | (E2) hanger detall |

## Floor Details

## (E3) I-JOIST HEADER



See 1-Joist Header CrossSection for information on attaching web fillers and filler blocks

## E4 I-JOIST HEADER CROSS SECTION

Filler Blocks: Fasten I-Joists together with filler blocks between the PWI webs:

- Filler blocks must be installed at any load that is not applied to the top of the member and equally to all plies. See Detail E5 for installation instructions.
- For joists supporting only top loads that are equally applied to both plies, filler blocks can be omitted.

Backer Blocks: Minimum 12" long backer blocks must be installed at all hangers and all concentrated loads that are not equally applied to
 each ply, center backer block on load.

- For a single I-joist header install backer blocks to both sides of the web.
- Backer blocks may be omitted for top-mount hangers supporting only downward loads not exceeding 250 lbs.
- Install backer blocks tight to top flange for top-mount hangers or top concentrated loads. Install tight to bottom flange for face-mount hangers.
- Attach using 10 nails ( $0.131^{\prime \prime \times 3-1 / 4 " ~(m i n .), ~ c l i n c h ~ w h e r e ~ p o s s i b l e) ~ s p a c e d ~ t o ~ a v o i d ~ s p l i t i n g, ~ w i t h ~}$ half the nails to each side of the center of the supported hanger.
- Face mount hanger nails must be min. $3^{3}$ long per manufacturer's specifications.


## Filler and Backer Blocks:

- Refer to the l-Joist Filler Thickness table for the correct filler and backer block thickness.
- Filler and backer blocks shall consist of APA Rated wood structural panel (OSB or plywood), 2 x lumber (SPF or better), or PWT LVL or OSB Rim Board.
- Filler and backer blocks for members that are top-loaded only, or at hangers that do not require nailing into the web, shall be: at least $5-1 / 2^{\prime \prime}$ deep for 1 -joists up to $11-7 / 8^{" 1}$ deep and at least $7-1 / 4^{\prime \prime}$ deep for 1 -joists deeper than $11-7 / 88^{\prime \prime}$. Otherwise, filler blocks shall fit the clear distance between flanges with a gap of at least $1 / 8$ ", but not more than 1 ".
- For double PWIs that are not top loaded or have loads that are not applied equally to both plies, the max unfactored loads for standard duration: Concentrated Load = 1200 lbs . Uniform Load = 520 plf. Loads may be increased with more nails and adjusted for other load durations.

Contact the project's design professional or a PWT distributor if these conditions are not met.

## Filler Block Depth Example:

Multiple filler blocks may be stacked vertically to achieve the filler depth for a 14 " deep I-joist (min. req. is $14^{\prime \prime}-3^{\prime \prime}-1 "=10 "$ ). One row of nails must be in each filler.

Backer Block Length Example:
Two pieces, example $2 \times 8$ (min.) lumber, that are cut to the proper height may be set vertically side-by-side to achieve the required minimum 12 length.

- Joists $\leq 2-1 / 2$ " thick: from either side, total of 10 nails
- Joists > 2-1/2" thick: from each side, total of 20 nails

Stagger rows, clinch where possible, and spaced to avoid spliting.

Refer to 1 -Joist Filler
Thickness table for web filler (backer block) and filler block sizes

## E5 DOUBLE I-JOIST CONNECTION



Refer to l-Joist Filler Thickness table for filler block sizes

Filler blocks must be:

- Long enough not to split when nailed (12" min.)
- Located at each support
- Under all concentrated loads that are not equally applied to each ply
- Centered behind each hanger
- At 24" oc max. under all uniform loads that are not equally applied to each ply
- Installed tight to top flange at top-mount hangers and top concentrated loads.
- Installed tight to bottom flange at supports and facemount hangers.

Floor sheathing to be glued and nailed to flanges of both plies
Attach using ten (10) $0.131^{\prime \prime} \times 3-1 / 4$ " nails (min.):

## I-JOIST FILLER THICKNESS

| Span (ft) | Filler Block | Web Filler/Backer Block |
| :---: | :---: | :---: |
| PWI 18S, LPI 18, <br> PWI 20S, LPI 20Plus <br> PWI 32S, LPI 32Plus | $2-1 / 8^{\prime \prime}$ | $1^{\prime \prime}$ |
| PWI 36L, LPI 36 | $1-7 / 8^{\prime \prime}$ | $7 / 8^{\prime \prime}$ |
| PWI 42S, LPI 42PluS <br> PWI 52S, LPI 52Plus <br> PWI 56L, LPI 56 | $3 "$ | $1-1 / 2^{\prime \prime}$ |

## Notes:

1. Backer blocks and filler blocks shall consist of APA Rated wood structural panel (OSB or plywood), or $2 x$ lumber (SPF or better).
2. OSB or PWT LVL Rim may also be used
3. Refer to the Notes for the 1 -Joist Header Cross-Section above for details on the required height and length, and nailing of the backer blocks and filler blocks.

## General Notes:

1. Some wind or seismic loads may require different or additional details and connections.
2. Verify building code requirements for suitability of details shown.
3. Refer to page 4 for bearing length requirements.
4. Refer to page 25 for Flange Face Nailing Schedule for PWI rim joist or blocking panel nailing.
5. Lateral support shall be considered for bottom flange when there is no sheathing on underside.
6. Verify capacity and fastening requirements of hangers and connectors.
7. Squash block capacity designed by others.
8. Do not use PWI joists with flanges wider than $2-1 / 2$ "as rim joists.

## Roof Details



## Framing Connectors <br> General Notes:

1. The following tables provide a list of the more common hangers and connectors for use with PWT ${ }^{m \times \prime}$ I-Joists.
2. Refer to the manufacturer's connector guide for a complete list of hangers and to verify the suitability of a hanger or connector for a particular application.
3. Follow all connector manufacturers' installation guidelines.

## SIMPSON STRONG-TIE ${ }^{\ominus}$

| Series | Depth | Top-Mount |  | Face-Mount |  | $\begin{gathered} \hline 45^{\circ} \text { Skewed } \\ \hline \text { Single } \\ \hline \end{gathered}$ | Field Slope \& Skew <br> Single | Variable Pitch Seat Single |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Single | Double | Single | Double |  |  |  |
| 2-1/2" Flange (PWI 18S, LPI 18, PWI 20S, LPI 20Plus, PWI 32S, LPI 32Plus) | 9-1/2" | ITS2.56/9.5 | MIT39.5-2 | IUS2.56/9.5 | MIU5.12/9 | SUR/L2.56/9 | LSSUH310* | VPA3 |
|  | 11-7/8" | ITS2.56/11.88 | MIT311.88-2 | IUS2.56/11.88 | MIU5.12/12 | SUR/L2.56/11 | LSSUH310* | VPA3 |
|  | 14 " | ITS2.56/14 | MIT314-2 | IUS2.56/14 | MIU5.12/14 | SUR/L2.56/14 | LSSUH310* | VPA3 |
|  | 16" | ITS2.56/16 | MIT5.12/16 | IUS2.56/16 | MIU5.12/16 | SUR/L2.56/14* | ** | VPA3 |
| 2-1/4" Flange (PWI 36L, LPI 36) | 11-7/8" | ITS2.37/11.88 | MIT3511.88-2 | IUS2.37/11.88 | MIU4.75/11 | SUR/L2.37/11 | LSSUI35* | VPA35 |
|  | $14 "$ | ITS2.37/14 | MIT3514-2 | IUS2.37/14 | MIU4.75/14 | SUR/L2.37/14 | LSSUI35* | VPA35 |
|  | $16 "$ | ITS2.37/16 | MIT4.75/16 | IUS2.37/16 | MIU4.75/16 | SUR/L2.37/14* | ** | VPA35 |
| 3-1/2" Flange (PWI 42S, LPI 42Plus, PWI 52S, LPI 52Plus, PWI 56L, LPI 56) | 9-1/2" | ITS3.56/9.5 | B7.12/9.5 * | IUS3.56/9.5 | HU410-2* | SUR/L410* | LSSU410* | VPA4 |
|  | 11-7/8" | ITS3.56/11.88 | B7.12/11.88 * | IUS3.56/11.88 | HU412-2* | SUR/L410 * | LSSU410* | VPA4 |
|  | $14 "$ | ITS3.56/14 | B7.12/14 * | IUS3.56/14 | HU414-2* | SUR/L414* | LSSU410* | VPA4 |
|  | 16" | ITS3.56/16 | B7.12/16 * | IUS3.56/16 | HU414-2* | SUR/L414 * | ** | VPA4 |

* Web filler required for proper installation of hanger.
** Refer to Simpson Strong-Tie "Wood Construction Connectors" catalog for hanger selection.

MITEK ${ }^{\circledR}$ STRUCTURAL CONNECTORS

| Series | Depth | Top-Mount |  | Face-Mount |  | $\begin{gathered} 45^{\circ} \text { Skewed } \\ \hline \text { Single } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Field Slope \& Skew } \\ \hline \text { Single } \\ \hline \end{gathered}$ | Variable Pitch Seat Single |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Single | Double | Single | Double |  |  |  |
| 2-1/2" Flange (PWI 18S, LPI 18, PWI 20S, LPI 20Plus, PWI 32S, LPI 32Plus) | 9-1/2" | TFL2595 | TH025950-2* | THF25925 | THF25925-2* | SKH2520L/R* | LSSH25 * | TMP25 or TMPH25 * |
|  | 11-7/8" | TFL25118 | TH025118-2* | THF25112 | THF25112-2* | SKH2520L/R* | LSSH25* | TMP25 or TMPH25 * |
|  | $14 "$ | TFL2514 | TH025140-2* | THF25140 | THF25140-2* | SKH2524L/R* | LSSH25 * | TMP25 or TMPH25 * |
|  | 16 " | TFL2516 | TH025160-2* | THF25160 | THF25160-2* | SKH2524L/R* | LSSH25 * $\dagger$ | TMP25 or TMPH25* |
| 2-1/4" Flange (PWI 36L, LPI 36) | 11-7/8" | TFL23118 | TH023118-2* | THF23118 | THF23118-2* | SKH2320L/R* | LSSH23* | TMP23 or TMPH23* |
|  | $14 "$ | TFL2314 | TH023140-2* | THF23140 | THF23140-2* | SKH2324L/R* | LSSH23 * | TMP23 or TMPH23 * |
|  | $16 "$ | TFL2316 | TH023160-2* | THF23160 | THF23160-2* | SKH2324L/R* | LSSH23 * $\dagger$ | TMP23 or TMPH23 * |
| 3-1/2" Flange (PWI 42S, LPI 42Plus, PWI 52S, LPI 52Plus, PWI 56L, LPI 56) | 9-1/2" | TH035950 | BPH7195* | THF35925 | HD7100 * | SKH410L/R*** | LSSH35* | TMP4 or TMPH4 * |
|  | 11-7/8" | TH035118 | BPH71118* | THF35112 | HD7120* | SKH410L/R*** | LSSH35* | TMP4 or TMPH4 * |
|  | $14 "$ | TH035140 | BPH7114* | THF35140 | HD7140* | SKH414L/R*** | LSSH35* | TMP4 or TMPH4 * |
|  | $16 "$ | TH035160 | BPH7116* | THF35157 | HD7160 * | SKH414L/R*** | LSSH35 * $\dagger$ | TMP4 or TMPH4 * |

[^3]Top-Mount
Face-Mount

## Web Stiffeners, Rim \& Blocking, Nailing

## WEB STIFFENER DETAILS



Nails to be equally spaced, staggered and driven alternately from each face. Clinch nails where possible.
*Refer to framing plan for specific conditions.

## Notes:

1. Web stiffeners shall be installed in pairs - one to each side of the web. Web stiffeners are always required for the "Bird's Mouth" roof joist bearing detail.
2. Web stiffeners shall be cut to fit between the flanges of the PWTT" 1 -Joist, leaving a minimum $1 / 8^{\prime \prime}$ gap ( $1^{\prime \prime}$ maximum). At bearing locations, the stiffeners shall be installed tight to the bottom flange. At locations of concentrated loads, the stiffeners shall be installed tight to the top flange.
3. Web stiffeners shall be cut from APA Rated OSB (or equal) or from PWT LVL or OSB Rim Board. $2 x$ lumber is permissible. Do NOT use $1 x$ lumber as it tends to split. Do NOT build up the required stiffener thickness from multiple pieces.
4. Web stiffeners shall be the same width as the bearing surface, with a minimum of $3-1 / 2$."
5. See Web Stiffener Requirements for minimum stiffener thickness, maximum stiffener height and required nailing.

## WEB STIFFENER REQUIREMENTS

| Series | Depth | Minimum Thickness | Maximum Height | Nail Size* | Nail Quantity |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PWI 18S, LPI 18PWI 20S, LPI 20PIUS PWI 32S, LPI 32Plus | 9-1/2" | 23/32 | 6-3/8" | 8d (2-1/2") | 3 |
|  | 11-7/8" | 23/32 | 8-3/4" | 8d (2-1/2") | 3 |
| $\begin{aligned} & \text { PWI 20S, LPI 20Plus } \\ & \text { PWI 32S, LPI 32Plus } \end{aligned}$ | 14 | 23/32 | 10-7/8" | 8d (2-1/2") | 3 |
|  | $16 "$ | 23/32 | 12-7/8" | 8d (2-1/2") | 3 |
| PWI 36L, LPI 36 | 11-7/8" | 23/32 | 8-3/4" | 8d (2-1/2") | 4 |
|  | 14 | 23/32 | 10-7/8" | 8d (2-1/2") | 5 |
|  | $16 "$ | 23/32 | 12-7/8" | 8d (2-1/2") | 6 |
| PWI 42S, LPI 42Plus | 9-1/2" | 1-1/2 | 6-3/8" | 10d (3") | 3 |
| PWI 42S, LPI 42Plus PWI 52S, LPI 52Plus | 11-7/8" | 1-1/2 | 8-3/4" | 10 d (3") | 3 |
|  | 14" | 1-1/2 | 10-7/8" | 10 d (3") | 3 |
|  | $16 "$ | 1-1/2 | 12-7/8" | 10 d (3") | 3 |
| PWI 56L, LPI 56 | 11-7/8" | 1-1/2 | 8-3/4" | 10d (3") | 4 |
|  | $14 "$ | 1-1/2 | 10-7/8" | 10d (3") | 5 |
|  | $16 "$ | 1-1/2 | 12-7/8" | 10 d (3") | 6 |

*Nails may be Box or Common.

## RIM \& BLOCKING CAPACITY

| Series | Depth | Factored Vertical <br> Resistance (plf) |
| :---: | :---: | :---: |
| PWI 18S, LPI 18 | $9-1 / \mathbf{2}^{\prime \prime}$ | 2755 |
| PWI 20S, LPI 20Plus | $\mathbf{1 1 - 7 / 8 "}$ | 2552 |
| PWI 20S, LPI 20Plus | $\mathbf{1 4 "}$ | 2320 |
|  | $\mathbf{1 6 "}$ | 2175 |
| PWI 32S, LPI 32Plus | $\mathbf{9 - 1 / 2 "}$ | 3190 |
| PWI 42S, LPI 42Plus | $\mathbf{1 1 - 7 / 8 "}$ | 3190 |
|  | $\mathbf{1 4 "}$ | 2320 |
|  | $\mathbf{1 6 "}$ | 2175 |
| PWI 36L, LPI 36 | $\mathbf{1 1 - 7 / 8 "}$ | 2610 |
|  | $\mathbf{1 4 "}$ | 2610 |
| PWI 52S, LPI 52Plus | $\mathbf{1 6 "}$ | 2610 |
| PWI 56L, LPI 56 | $\mathbf{1 1 - 7 / 8 "}$ | 3480 |
|  | $\mathbf{1 4 "}$ | 3190 |

## Notes:

1. The Factored Vertical Resistance is the capacity in pounds per lineal foot of length (plf) and shall not be adjusted for load duration.
2. Concentrated vertical loads require the addition of squash blocks. Do not use PWI rim or blocking to support concentrated vertical loads.
3. Lateral load capacity for all series above is 200 plf but may be limited by the connection details used. Do not exceed the Flange Face Nailing requirements at right.

## FLANGE FACE NAILING

| Series | Common Wire Nail Size | Minimum Nail Distance |  |
| :---: | :---: | :---: | :---: |
|  |  | oc Spacing | End |
| PWI 18S, LPI 18 PWI 20S, LPI 20Plus PWI 32S, LPI 32Plus PWI 42S, LPI 42Plus PWI 52S, LPI 52Plus | 2-1/2" | $2 "$ | 1" |
|  | 3" | $3 "$ | 1-1/2" |
|  | 3-1/4" | 3" | 1-1/2" |
|  | 3-1/2" | 4" | 1-1/2" |
| PWI 36L, LPI 36 <br> PWI 56L, LPI 56 | 2-1/2" | 3" | 1-1/2" |
|  | 3" | 3" | 1-1/2" |
|  | 3-1/4" | $3 "$ | 1-1/2" |
|  | 3-1/2" | 5" | 1-1/2" |

Notes:

1. Use only $2-1 / 2$ " or 3 " nails when securing an PWI floor or roof joist to its supports.
2. Power-driven nails shall have a yield strength equivalent to common wire nails of the same shank diameter.

NAIL NAMES AND SIZES

| Callout | Common Name | Min. Length | Diameter |
| :---: | :---: | :---: | :---: |
| 8d | box | $2-1 / 2^{\prime \prime}$ | $0.113^{\prime \prime}$ |
|  | common | $2-1 / 2^{\prime \prime}$ | $0.131^{\prime \prime}$ |
| 10d | box | $3^{\prime \prime}$ | $0.128^{\prime \prime}$ |
|  | common | 3 " | $0.148^{\prime \prime}$ |
| 16d | box | $3-1 / 2^{\prime \prime}$ | $0.135^{\prime \prime}$ |
|  | common | $3-1 / 2^{\prime \prime}$ | $0.162^{\prime \prime}$ |

## Notes:

1. Common nails are assumed unless otherwise indicated.
2. 10d box may be substituted for 8 d common nails.

## Rim Board

## FACTORED RIM BOARD RESISTANCE

| Material | Grade | Thickness | Vertical Load Resistance |  |  | Lateral ${ }^{14,5}$ Load Capacity (plf) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Uniform |  | Concentrated |  |
|  |  |  | d $\leq 16{ }^{\prime \prime}$ | $16^{\prime \prime}<d \leq 24 "$ | d $\leq 24{ }^{\prime \prime}$ |  |
| OSB | APA C1/Rim Board7 | 1-1/8" | 7033 | 4640 | 5075 | 219 |

## Notes:

1. The Factored Vertical Load Resistance shall not be increased for short-term load duration.
2. The Factored Vertical Load Resistance is based on the resistance of the rim board and may need to be reduced based on the bearing resistance of the supporting wall plate or the attached floor sheathing.
3. The Factored Concentrated Vertical Load Resistance is assumed to be applied through a minimum 4-1/2" bearing length (3-stud post).
4. The Factored Lateral Load Resistance is based on a short-term load duration and shall not be increased.
5. The Factored Lateral Load Resistance is based on the connections specified in the Installation details below.
6. Additional framing connectors fastened to the face of the rim board may be used to increase lateral resistance for wind and seismic design.
7. APA C1 grade in product standard ANSI/APA PRR 410 is equivalent to the rim board grade in product standard APA PRR-401C.

## FACTORED UNIFORM LOADS (PLF) FOR RIM BOARD HEADERS: MAXIMUM 4' CLEAR SPAN

| Material | Thickness | Rim Board Depth |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1-1 / 8^{\prime \prime}$ | $9-1 / 2^{\prime \prime}$ | $620\left(3^{\prime \prime}\right)$ | $11-7 / 8^{\prime \prime}$ | $965\left(3^{\prime \prime}\right)$ |
| OSB |  | $2220\left(4-1 / 2^{\prime \prime}\right)$ | $2535\left(4-1 / 2^{\prime \prime}\right)$ |  |  |

## Notes:

1. This table is for preliminary design for uniform gravity loads only. Final design should include a complete analysis of all loads and connections.
2. The factored load resistances are for a maximum 4' clear span with minimum bearings for each end (listed in parentheses) based on the bearing resistance of the rim board. For headers bearing on wood plates, the bearing length may need to be increased based on the ratio of the bearing resistance of the rim board divided by the bearing resistance of the plate species.
3. Standard load duration is assumed and shall be adjusted according to code.
4. Depths greater than $11-7 / 8$ " shall be used with a minimum of two plies, as shown. Depths of $11-7 / 8$ " and less may be used as a two-ply header by multiplying the resistance by two.
5. Multiple-ply headers shall be toe-nailed to the plate from both faces. Fasten the floor sheathing to the top of each ply to provide proper lateral support for each ply.
6. For multiple-ply headers supporting top-loads only, fasten plies together with minimum 2-1/2" nails (common wire or spiral) at a maximum spacing of $12^{\prime \prime}$ oc. Use 2 rows of nails for $9-1 / 2^{\prime \prime}$ and 11-7/8". Use 3 rows for depths 14 " and greater. Clinch the nails where possible. For side-loaded multiple-ply headers, refer to the Connection Resistance For Side-Loaded 2-Ply Rim Board Headers table below for the required nailing and the maximum side load that can be applied.
7. The designer shall verify proper bearing for the header.
8. Joints in the rim are not allowed over openings and must be located at least 12 " from any opening.
9. Refer to the "APA Performance Rated Rim Boards - Limit States Design" (Form No. D340 CA) for additional information including uniform load resistance for smaller openings.

## FACTORED CONNECTION RESISTANCE FOR SIDE-LOADED 2-PLY RIM BOARD HEADERS (PLF)

| Material | Thickness | Minimum Nail Size at 6 " oc | 3 Rows of Nails at 6 " oc | 4 Rows of Nails at 6" oc | 5 Rows of Nails at 6" oc | 6 Rows of Nails at 6" oc |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OSB | 1-1/8" | 2-1/2" | 1280 | 1707 | 2134 | 2561 |

## Notes:

1. This table represents the factored uniform side-load resistance of the connection for a 2-ply header. The total factored uniform load, including top-load and side-load, shall not exceed the factored uniform load resistance of the header as tabulated above.
2. The tabulated side-load resistance is for standard load duration and shall be adjusted according to code.
3. Use 3 rows of nails for $9-1 / 2^{\prime \prime}$ and $11-7 / 8^{\prime \prime} ; 4$ rows for $14^{\prime \prime}$ and $16^{\prime \prime} ; 5$ rows for $18^{\prime \prime}$ and $20 " ; 6$ rows for $22^{\prime \prime}$ and 24 " deep rim board.
4. Nails may be either common wire or spiral. The factored resistances are based on spiral nails. Clinch the nails where possible.
5. Headers consisting of more than 2 plies, alternate fastening or higher side loads are possible but require proper design of the connection.

## INSTALLATION

RIM TO JOIST CONNECTION


Nail rim to I-Joist with one 8d (box or common) or 10d box nail into each flange.

DECK TO RIM AND RIM TO PLATE CONNECTIONS¹



T\&G TRIM REQUIREMENTS

| Floor Sheathing <br> Thickness | Rim Board Thickness |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{1 "}^{\prime \prime}$ | $1-1 / 8^{\prime \prime}$ | $1-1 / 4^{\prime \prime}$ | $>1-1 / 4^{\prime \prime}$ |
| $\leq 7 / 8^{\prime \prime}$ | Trim | Not Required | Not Required | Not Required |
| $>7 / 8^{\prime \prime}$ | Trim | Trim | Trim | Not Required |

## Warnings



## W ARNINGS

The following conditions are NOT permitted!
Do not use visually damaged products without first checking with your local PWT ${ }^{T M}$ distributor or sales office.
DON'T put holes too close to supports.

## Handling and Storage

## HANDLING AND STORAGE GUIDELINES

- WARNING: Failure to follow proper procedures for handling, storage and installation could result in unsatisfactory performance, unsafe structures and possible collapse.
- Keep PWT ${ }^{T M}$ products dry. These products are intended to resist the effects of moisture on structural performance from normal construction delays but are not intended for permanent exposure to the weather.
- Unload products carefully, by lifting. Support the bundles to reduce excessive bowing. Individual products should be handled in a manner which prevents physical damage during measuring, cutting, erection, etc. I-Joists shall be handled vertically and not flatwise.
- Keep products stored in wrapped and strapped bundles, stacked no more than 10 high. Support and separate bundles with $2 \times 4$ (or larger) stickers spaced no more than 10' apart. Keep stickers in line vertically.
- Product must not be stored in contact with the ground, or have prolonged exposure to the weather.
- Use forklifts and cranes carefully to avoid damaging product.
- Do not use a visually damaged product. Call your local PWT distributor for assistance when damaged products are encountered.
- For satisfactory performance, PWT I-Joists and LVL must be used under dry, covered and well-ventilated interior conditions in which the average equilibrium moisture content (MC) of lumber is $15 \%$ or less over a year and does not exceed $19 \%$ at any time.
- For built-up members, PWT I-Joists and LVL shall be dry before nailing or bolting to avoid trapping moisture.
- PWT ${ }^{m \times 1}$ I-Joists and LVL shall not be used for unintended purposes such as ramps and planks.


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[^0]:    * Deflections rounded to the nearest 1/16.

[^1]:    * Deflections rounded to the nearest $1 / 16$."

[^2]:    *Deflections rounded to the nearest $1 / 16$.

[^3]:    * Web filler required for proper installation of hanger.
    ** Miter cut required on end of joist.
    $\dagger$ Hanger height is less than $60 \%$ of the joist depth. Supplemental lateral support of the top flange is required. Refer to MiTek's installation instructions.

    1. Use TMP seats for joist pitch of 1:12 to 6:12. Use TMPH for joist pitch of 6:12 and greater.
